Optical bend sensor based on a long-period fiber grating monitored by an optical time-domain reflectometer

Orlando Frazão
Instituto de Engenharia de Sistemas e Computadores do Porto (INESC-Porto)
Rua do Campo Alegre, 687
4169-007 Porto, Portugal

Rosane Falate
INESC-Porto
Rua do Campo Alegre, 687
4169-007 Porto, Portugal
and
Centro Federal de Educação Tecnológica do Paraná
80230-901 Curitiba, Brazil

Jose M. Baptista
INESC-Porto
Rua do Campo Alegre, 687
4169-007 Porto, Portugal
and
Instituto de Engenharia do Porto
Dep. de Engenharia Electro-técnica
Rua Dr. António Bernardino de Almeida, 431
4200-072 Porto, Portugal

Jose L. Fabris
Centro Federal de Educação Tecnológica do Paraná
80230-901 Curitiba, Brazil

Jose L. Santos, MEMBER SPIE
INESC-Porto
Rua do Campo Alegre, 687
4169-007 Porto, Portugal
and
Universidade do Porto
Faculdade de Ciências
Departamento de Física
Rua do Campo Alegre, 687
4169-007 Porto, Portugal

Abstract. We report an alternative technique to interrogate a long-period fiber grating (LPG) when the grating sensitivity is based on the peak amplitude changes of the resonant wavelength. To read the amplitude changes, a conventional optical domain reflectometer was used. Bend measurements were performed to apply such method and to determine the grating sensitivity for this physical parameter. Reflective measurements, temperature insensitive, and the possibility of multiplexing LPG sensors are some advantages offered by this technique. © 2005 Society of Photo-Optical Instrumentation Engineers. [DOI: 10.1117/1.2123267]

Subject terms: long-period fiber grating; OTDR; bend sensor.

Paper 050609LR received Jul. 27, 2005; revised manuscript received Aug. 19, 2005; accepted for publication Sep. 21, 2005; published online Nov. 10, 2005.

1 Introduction

A long-period fiber grating (LPG) is a periodic refractive index structure on the fiber core whose periodicity is in the range of several hundred micrometers. The large period of modulation promotes the optical coupling between the propagating core mode and copropagating cladding modes. Since the cladding modes, consequently the resonant peaks, are sensitive to the physical parameters, curvature or bending measurement can be performed utilizing LPGs. In fact, several authors have demonstrated the bending-induced wavelength shift by means of LPGs. However, the cross sensitivity when different physical parameters are changed at the same time continues to be a common problem of using this kind of grating structure as an optical sensor. Trying to surpass part of this problem, Ye et al. proposed a sensor head based on LPGs operating at short wavelengths for simultaneous measurement of temperature and bend.

Another problem with the usage of LPGs is the difficulty to interrogate its spectral response since the resonant bands have large bandwidth. Commonly an optical spectrum analyzer (OSA) is used, but this equipment is unpractical for real-time applications due to its size and high cost. Because of this, Allsop et al. proposed a new method for LPG interrogation based on derivative spectroscopy technique. In this work, we present an optical bend sensor that uses an LPG written by electric arc discharge and interrogated by a conventional optical time-domain reflectometer (OTDR). The proposed system detects the losses variation of the LPG when the bend is applied and permits a stable measurement independent of temperature fluctuation. A multiplexing experiment using two LPGs in series was also demonstrated.

2 Experimental Results

An LPG with a period $\Lambda=540 \mu m$ and length $L_{LPG}=21.6 \text{ mm}$ was arc-induced in Corning SMF-28 fiber. During the grating inscription, the fiber was kept under a tension of 5.1 g, and was subjected to 40 arc discharges with 9 mA of current and 1-s duration. With the OSA resolution set to 0.1 nm and a wavelength range from 1520 to 1570 nm, we first observed the transmission spectrum when the LPG was straight. The obtained central wavelength for this condition was 1557 nm. Second, for the bend tests, a section of fiber ($2L=330 \text{ mm}$) with a LPG in the middle was clamped between a translation stage (TS) and a fixed base. The sensor curvature $R$ is given by:

$$R=d/(d^2+L^2),$$

where $d$ is the bending displacement at the center of the LPG and $L$ is the half distance between the edges of the two clamps (see Fig. 1). Figure 2 shows the transmission spectrum of LPG when curvature is applied. We observed that the wavelength and the attenuation of the central peak are changed with the curvature.

To characterize the LPG sensitivity to the applied curvature without the OSA, we used a commercial OTDR to read the losses generated by the LPG (see Fig. 1). In this experience, the optical bend sensor was placed between two optical fiber rolls (SMF 28) with lengths of 3500 and 100 m, respectively. The loss of the LPG sensor is measured using the internal multimode laser of OTDR with...
Fig. 1 Experimental setup using an OTDR.

Fig. 2 Bend sensitivity of LPG obtained by an optical spectrum analyzer.

Fig. 3 LPG response observed by the OTDR when curvature is applied for: (a) $R=2.3$ m$^{-1}$ and (b) $R=5.5$ m$^{-1}$.

Fig. 4 Evolution of LPG amplitude loss against curvature.

Fig. 5 LPG amplitude loss insensitivity to temperature for a fixed curvature of 2.8 m$^{-1}$.

Fig. 6 OTDR measurement when bending two LPGs in series.
pulses of 100 ns and working at 1550 nm. When the LPG is illuminated by the laser pulse, the LPG resonance near 1550 nm increased the backscattering, which was sent in reflection, and was analyzed by the OTDR. Since the peak amplitude loss of the LPG sensor increases when curvature is applied, a higher backscattering is produced at the LPG location that is detected by the OTDR. The opposite amplitude sensitivity of LPG for curvature increment is observed because the LPG is working in the recoupling mode region.

Figure 3 shows the OTDR measurements for two different applied curvatures on the LPG. The valley and the peak at 3500 m correspond to the loss of the LPG sensor and the Fresnel reflection, respectively. It can be observed that the valley goes deeper as a result of the curvature increments [from Fig. 3(a) to 3(b)] while the fiber backscattering before the LPG is the same, being our reference point. This result shows that when the attenuation peak of LPG increases, the valley attenuation also increases.

Figure 4 presents the relationship between the loss and the curvature of the LPG. The loss values were obtained using two markers given by the OTDR. They are chosen to be located before (reference point) and at the LPG loss. For a curvature range between 2.0 and 5.5 m⁻¹, it obtained an amplitude loss shift of more than 4 dB. Figure 4 also shows two different regions of the LPG response. The first is a linear region, up to 3.5 m⁻¹, with a sensitivity of 2.16 dB/m⁻¹ and a maximum error of ±0.02 dB/m⁻¹. The other region shows a loss saturation of the LPG since the LPG reaches the maximum amplitude loss when the curvature is applied. After this loss saturation region, for curvature values higher than 5.5 m⁻¹, the LPG mode energy is recoupled and the amplitude loss decreases. This behavior limits the measurement range to the presented set of curvature measurements. However, such limitation is intrinsic to the LPG sensor. To surpass this, a new LPG design is necessary to increase the curvature range.

To confirm that this technique is temperature insensitive, since the spectral dependence on temperature of the LPG is almost in wavelengths, we inserted the LPG sensor in an oven with a curvature of 2.8 m⁻¹. The LPG was subject to a curvature range between 2.0 and 5.5 m⁻¹, it obtained an amplitude loss shift of more than 4 dB. Figure 4 also shows two different regions of the LPG response. The first is a linear region, up to 3.5 m⁻¹, with a sensitivity of 2.16 dB/m⁻¹ and a maximum error of ±0.02 dB/m⁻¹. The other region shows a loss saturation of the LPG since the LPG reaches the maximum amplitude loss when the curvature is applied. After this loss saturation region, for curvature values higher than 5.5 m⁻¹, the LPG mode energy is recoupled and the amplitude loss decreases. This behavior limits the measurement range to the presented set of curvature measurements. However, such limitation is intrinsic to the LPG sensor. To surpass this, a new LPG design is necessary to increase the curvature range.

Acknowledgments

R. Falate has her work supported in part by Coordenação de Aperfeiçoamento de Pessoal de Nível Superior (CAPES), Grant BEX: 0301/04-3, Brazilian Agency.

References