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Abstract. Three aluminum (Al)/silicon dioxide (SiO$_2$)/aluminum (Al) nanosandwich films (SWFs) of various heights were fabricated using glancing angle deposition. An SWF comprises a 45-nm thick SiO$_2$ layer sandwiched between two Al nanopillars. The thicknesses of both top and bottom nanopillars were varied from 187.5 to 217.5 nm. The equivalent constitutive and related parameters of each SWF were obtained from the reflection coefficients and transmission coefficients that were measured using a walk-off interferometer. Both the equivalent permittivity and the equivalent permeability of each SWF turned out to be negative real. Exactly how the height of the Al nanopillars of the double negative SWF affects its low reflectance through destructive interference is also examined using the wave tracing method. Moreover, the localized reversed magnetic field in the SiO$_2$ layer of each SWF was simulated by finite-difference time-domain method to qualitatively interpret the negative real permeability. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: 10.1117/1.JNP.8.083994]

Keywords: metamaterials; optical properties; thin films.

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1 Introduction

With the rapid development of metamaterials in the recent decade, related works have demonstrated the novel optical properties of subwavelength structures of such metamaterials, including the negative refractive index$^1$–$^3$—from microwave wavelengths to visible wavelengths. To achieve related applications (e.g., perfect lens and cloaking$^5$), many recent efforts have attempted to reduce the loss of metamaterials.$^5$ However, between the discovery of metamaterials and the development of metadevices, the mass production of metamaterials is of priority concern.$^7$ In addition to electron-beam lithography,$^8$ glancing angle deposition$^9$ is a relatively facile means of coating a nanostructured thin film with a negative refractive index at visible wavelengths. By depositing at a glancing angle of 89 deg and deposition rate of 1 nm/s, a slanted Ag nanorod array (NRA) with a thickness of 160 nm exhibits a negative real refractive index. Measurement results indicate that the polarization-dependent refractive index is positive real for s-polarization (i.e., the electric field of the incident wave oscillates normally to the rods) and negative real for p-polarization (i.e., the electric field of the incident wave oscillates along the rods). The p-polarized refractive index is $\lambda = 0.581 + i0.213$, $\lambda = 0.307 + i1.621$, and $\lambda = 0.389 + i1.816$ at wavelengths $\lambda$ of 532, 639, and 690 nm, respectively.$^10$ However, the p-polarization transmittance of Ag NRA is only <5%, owing to its strong light absorption.

A previous work attempted to mitigate the loss problem of metal NRA by fabricating a sandwiched Al–SiO$_2$–Al upright NRA was fabricated through the introduction of rapidly substrate spin during glancing deposition.$^{11}$ This sandwiched NRA exhibits a polarization-independent negative refractive index and equivalent permeability for normal incidence. Additionally, The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: 10.1117/1.JNP.8.083994] Keywords: metamaterials; optical properties; thin films.

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A previous work attempted to mitigate the loss problem of metal NRA by fabricating a sandwiched Al–SiO$_2$–Al upright NRA was fabricated through the introduction of rapidly substrate spin during glancing deposition.$^{11}$ This sandwiched NRA exhibits a polarization-independent negative refractive index and equivalent permeability for normal incidence. Additionally,
loss of the sandwiched film is sufficiently low to allow light to propagate through and to be reflected back from, the film, subsequently producing interference effect. Antireflection caused by destructive interference from the film is observed and demonstrated herein. The negative phase change caused by backward wave propagation in a negative index medium contributes to the destructive interference between the first two orders of reflected waves.

This work examines how the Al nanopillar thickness affects electromagnetic and optical properties of the Al–SiO$_2$–Al sandwiched. Three samples with Al nanopillar thicknesses varying from 187.5 to 217.5 nm are fabricated. Their electromagnetic parameters, including permittivity, permeability, and the bianisotropic parameter, are also derived from optical parameters, including refractive index, forward impedance, and backward impedance. The optical parameters are derived from the reflection and transmission coefficients measured by using walk-off interferometry. Moreover, the low reflectance values for different thicknesses of nanosandwich films (SWFs) are analyzed using the optical parameters. Furthermore, the negative real permeability variation with the size of SWF is investigated through simulation of the localized magnetic field, by using the finite-difference time-domain (FDTD) method. This work reveals that low reflectivity exists over an extended range of thickness of SWF with negative real index. The thickness-dependent optical parameters will be useful in optical thin film design for a novel optical filter that contains both positive and negative index thin films.

2 Fabrication and Measurement

In the fabrication of SWF, SWFs were grown by glancing angle deposition (GLAD) technique in an electron-beam evaporation system. The chamber containing the substrates and the targets of aluminum and silicon dioxide was pumped to a base pressure of $4 \times 10^{-6}$ Torr prior to evaporation. The target-to-substrate distance was fixed at 29 cm. The collimated vapor flux of either Al or SiO$_2$ was directed toward the substrate at an angle of 89 deg to the substrate normal. The substrate spun around its central normal axis at a rate of 10 rpm, subsequently causing the growing film to comprise upright nanopillars. A quartz crystal microbalance was placed next to the stage to monitor the deposition rate, which was maintained at approximately 1 nm/s. Figure 1 presents the top-view and cross-section views of the three SWFs. Table 1 lists the size parameters, including the average diameter and average thickness of each SWF.

Figure 1 describes the system coordinates $(x, y, z)$, as defined for optical measurements, where the $z$-axis is the direction of normal to the surface of the film. According to Fig. 2, the $(x,y)$-polarized transmittance $T_j$, reflectance $R_j$, and absorbance $A_j = 1 - (R_j + T_j)$, $j \in \{x, y\}$, of the SWF depends slightly on the orientation of the electric field of normally incident light. Here, the spectra of both transmittance and reflectance are measured on a TRIAX 180 spectrometer (Horiba Jobin Yvon, Opticsvalley, France). The transmittance of all three samples increases with wavelength, and a thicker SWF exhibits lower transmittance. The transmittance of the 420-nm thick SWF increases from 0.312 at $\lambda = 400$ nm to 0.687 at $\lambda = 700$ m, while the transmittance of the 480-nm thick SWF increases from 0.263 at $\lambda = 400$ nm to 0.627 at $\lambda = 700$ nm. Although the thickness of SWF varies from 420 to 480 nm, the reflectance levels of three samples are <1%.

**Fig. 1** Top view and cross-sectional scanning electron microscopic images of three Al – SiO$_2$ – Al nanosandwich films (SWFs) with total thicknesses of (a) 420 nm, (b) 450 nm, and (c) 480 nm, respectively.
The equivalent refractive index \( N_j = N_0 + jN_00 \), equivalent relative impedance \( Z_{+;j} = Z_{0;+} + jZ_{00;+} \) and \( Z_{-;j} = Z_{0;-} + jZ_{00;-} \) are derived from reflection and transmission coefficients measured from both sides of the air/SWF/substrate system using a method described elsewhere.\(^{12}\) The equivalent relative impedances \( Z_{+;j} = Z_{0;+} + jZ_{00;+} \) and \( Z_{-;j} = Z_{0;-} + jZ_{00;-} \) are associated with forward (+) and backward (−) directions of light propagating through the air/SWF/BK7 glass system (Fig. 1). The equivalent relative permittivity \( \varepsilon_j = \varepsilon_0 + j\varepsilon_00 \) and equivalent relative permeability \( \mu_j = \mu_0 + j\mu_00 \) are then calculated from \( N_j, Z_{+;j}, \) and \( Z_{-;j} \), respectively. Additionally, the complex-valued reflection coefficients \( r_{+;j} \) and transmission coefficients \( t_{+;j} \) of the SWF are measured for the SWF deposited on the glass slide, by using a walk-off interferometer with a wavelength-tunable 35 KAP 431-220 Ion Laser System (CVI MellesGriot, Albuquerque). The measurements are also taken at three wavelengths: 476, 568, and 676 nm. Figure 3 plots the values of \( N_j \) at the three wavelengths and Table 2 lists the values \( Z_{+;j} \) and \( Z_{-;j} \). Figure 4 presents the equivalent electromagnetic parameters and optical parameters of the three samples. The magnitude of the real part of the refractive index increases with wavelength, subsequently preventing the optical thickness

### Table 1 Average diameter and thickness of each sample.

<table>
<thead>
<tr>
<th>Sample</th>
<th>Total thickness of SWF (nm)</th>
<th>Thickness of SiO₂ layer (nm)</th>
<th>Thickness of Al layer (nm)</th>
<th>Average diameter (nm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>SWF-A</td>
<td>420</td>
<td>45.0</td>
<td>187.5</td>
<td>165.4</td>
</tr>
<tr>
<td>SWF-B</td>
<td>450</td>
<td>45.0</td>
<td>202.5</td>
<td>176.9</td>
</tr>
<tr>
<td>SWF-C</td>
<td>480</td>
<td>45.0</td>
<td>217.5</td>
<td>179.8</td>
</tr>
</tbody>
</table>

Light was normally incident for transmittance measurements, yet obliquely incident at 5 deg to the normal for reflectance measurements.

The equivalent refractive index \( N_j = N_j' + jN_j'' \), equivalent relative impedance \( Z_{+;j} = Z_{+;j}' + jZ_{+;j}'' \), and \( Z_{-;j} = Z_{-;j}' + jZ_{-;j}'' \) are derived from reflection and transmission coefficients measured from both sides of the air/SWF/substrate system using a method described elsewhere.\(^{12}\) The equivalent relative impedances \( Z_{+;j} = Z_{+;j}' + jZ_{+;j}'' \) and \( Z_{-;j} = Z_{-;j}' + jZ_{-;j}'' \) are associated with forward (+) and backward (−) directions of light propagating through the air/SWF/BK7 glass system (Fig. 1). The equivalent relative permittivity \( \varepsilon_j = \varepsilon_j' + j\varepsilon_j'' \) and equivalent relative permeability \( \mu_j = \mu_j' + j\mu_j'' \) are then calculated from \( N_j, Z_{+;j}, \) and \( Z_{-;j} \), respectively. Additionally, the complex-valued reflection coefficients \( r_{+;j} \) and transmission coefficients \( t_{+;j} \) of the SWF are measured for the SWF deposited on the glass slide, by using a walk-off interferometer with a wavelength-tunable 35 KAP 431-220 Ion Laser System (CVI MellesGriot, Albuquerque). The measurements are also taken at three wavelengths: 476, 568, and 676 nm. Figure 3 plots the values of \( N_j \) at the three wavelengths and Table 2 lists the values \( Z_{+;j} \) and \( Z_{-;j} \). Figure 4 presents the equivalent electromagnetic parameters and optical parameters of the three samples. The magnitude of the real part of the refractive index increases with wavelength, subsequently preventing the optical thickness
Table 2  \( Z_{\lambda;j} \) and \( Z_{-\lambda;j} \) for SWF-A, SWF-B, and SWF-C.

<table>
<thead>
<tr>
<th>Sample</th>
<th>( \lambda ) (nm)</th>
<th>( x )-polarization</th>
<th>( y )-polarization</th>
<th>( x )-polarization</th>
<th>( y )-polarization</th>
</tr>
</thead>
<tbody>
<tr>
<td>SWF-A</td>
<td>476</td>
<td>0.896 + /0.267</td>
<td>0.929 + /0.194</td>
<td>0.389 + /0.009</td>
<td>0.413 + /0.002</td>
</tr>
<tr>
<td></td>
<td>568</td>
<td>1.135 + /0.089</td>
<td>1.070 + /0.061</td>
<td>0.638 + /0.233</td>
<td>0.652 + /0.213</td>
</tr>
<tr>
<td></td>
<td>676</td>
<td>1.278 + /0.260</td>
<td>1.192 + /0.240</td>
<td>0.547 + /0.280</td>
<td>0.549 + /0.282</td>
</tr>
<tr>
<td>SWF-B</td>
<td>476</td>
<td>0.821 + /0.289</td>
<td>0.857 + /0.202</td>
<td>0.536 + /0.106</td>
<td>0.544 + /0.105</td>
</tr>
<tr>
<td></td>
<td>568</td>
<td>0.741 + /0.159</td>
<td>0.812 + /0.081</td>
<td>0.483 + /0.087</td>
<td>0.487 + /0.086</td>
</tr>
<tr>
<td></td>
<td>676</td>
<td>1.119 + /0.108</td>
<td>0.974 + /0.063</td>
<td>0.672 + /0.223</td>
<td>0.682 + /0.211</td>
</tr>
<tr>
<td>SWF-C</td>
<td>476</td>
<td>1.251 + /0.003</td>
<td>1.304 + /0.052</td>
<td>0.337 + /0.235</td>
<td>0.355 + /0.225</td>
</tr>
<tr>
<td></td>
<td>568</td>
<td>1.387 + /0.247</td>
<td>1.500 + /0.295</td>
<td>0.318 + /0.149</td>
<td>0.332 + /0.136</td>
</tr>
<tr>
<td></td>
<td>676</td>
<td>0.905 + /0.164</td>
<td>0.916 + /0.254</td>
<td>0.564 + /0.138</td>
<td>0.570 + /0.140</td>
</tr>
</tbody>
</table>

Fig. 4 Measured values of \( \varepsilon_j \) and \( \mu_j \) for SWF-A, SWF-B, and SWF-C.
varying intensively with wavelength. The imaginary part of the refractive index is sufficiently low to have interference between the first two reflected waves from SWF. The value $N_0^{\prime\prime}$ is within the range $(0.117, 0.137)$ for SWF-A, $(0.046, 0.073)$ for SWF-B, and $(0.086, 0.098)$ for SWF-C. As the thickness of SWF increases from 420 to 480 nm, the equivalent refractive index is negative; in addition, its average magnitude decreases from $-2.256$ to $-1.132$ at a wavelength $\lambda$ of 676 nm. Similarly, the real part of the equivalent permittivity varies from $-1.193$ to $-0.824$ as the thickness increases. Both equivalent permittivity and permeability are negative real, and the magnitude of the real part of the permeability increases as wavelength increases.

### 3 Wave Tracing

An attempt is made to exploit the cause of low reflectivity by using the equivalent optical parameters $N_x$, $Z_{+x}$, and $Z_{-x}$ to calculate the phase change associated with propagation through SWF, reflection coefficient, and transmission coefficient at both interfaces. The wave propagating through the film is simulated for two cases: the SWF-A at a wavelength of 676 nm and the SWF-C at a wavelength of 476 nm (Fig. 5). With incident electric field amplitude of unity, the first-order reflected wave and second-order reflected wave interfere with each other, resulting in a low reflectivity.
in diminished total reflected wave. The total reflected wave becomes $0.104e^{i(103.59^\circ)} + 0.144e^{i(-79.79^\circ)} = 0.041e^{i(88.44^\circ)} + 0.094e^{i(177.55^\circ)} = 0.058e^{i(2.27^\circ)}$ for SWF-C at a wavelength of 476 nm. Both cases perform well in terms of the destructive interference between the first two reflected waves from the SWF, owing to a low loss property of SWF. Owing to the negative real part of the refractive index, the phase associated wave propagation is negative as a result of backward wave propagation. The near-$\pi$ phase differences between the first-order and second-order reflected waves at wavelengths of 476 and 676 nm come from the low dispersive optical thickness, as shown in Sec. 2. Although the magnitude of the first-order reflection coefficient of SWF-A than that of SWF-C, the lower loss of SWF-A increases the magnitude of the second-order reflection coefficient of SWF-A more than that of SWF-C. Therefore, both cases have similar destructive interference phenomena.

4 Magnetic-Field Reversal Analysis

The negative real part of the permeability arises from the reversal of the magnetic field between a pair of aluminum grains. According to the values in Fig. 4, the average real part of the permeability of SWF-A varies from $-0.6684$ at $\lambda = 476$ nm, $-1.2878$ at $\lambda = 568$ nm to $-1.8588$ at $\lambda = 676$ nm. Additionally, the average real part of the permeability of SWF-B varies from $-0.6550$ at $\lambda = 476$ nm, $-0.9240$ at $\lambda = 568$ nm to $-1.5792$ at $\lambda = 676$ nm. Moreover, the average real part of the permeability of SWF-C varies from $-0.5361$ at $\lambda = 476$ nm, $-0.6183$ at $\lambda = 568$ nm to $-0.9240$ at $\lambda = 676$ nm. When the thickness of SWF increases from 420 to 450 nm, the magnitude of negative real permeability decays about 2.0%, 28.2%, and 15.1% at wavelengths of 476, 568, and 676 nm, respectively. However, the magnitude of the negative real part of the permeability obviously decays when the thickness increases from 450 to 480 nm; in addition, the value drops about 18.2%, 33.1%, and 41.5% at wavelengths of 476, 568, and 676 nm, respectively.

Reversal of the magnetic field in the SWF is induced by coupling in the dielectric layer of the antiphase electric fields that oscillate in the top and bottom nanodisks. Also, the magnitude of the negative real part of the permeability is proportional to that of the magnetic dipole moment. The magnetic response of individual sandwiches is simulated by the FDTD method for a sandwich model. The sandwich model consists of coaxial Al nanodisks, separated by a cylindrical SiO$_2$ spacer with a thickness of 45 nm. Since the diameter of the deposited Al nanopillar is a Gaussian distribution judged from the top-view SEM image, the diameter of Al nanodisk for simulation is varied over a range from 100 to 220 nm. The thickness of Al nanodisk is adopted, as determined by the average thicknesses of the three samples. Figure 6 plots the reversed magnetic field along the $y$-axis at the center of the spacer versus wavelength from 400 to 700 nm and the diameter of SWF ranging from 100 to 220 nm. Simulation results indicate that the reversal of the magnetic field occurs over the visible wavelengths when the diameter exceeds 160 nm. In the simulation of SWF-A, magnitude of the reversed magnetic field is the largest at a wavelength of 700 nm with the diameter of 180 nm. The other two simulations for SWF-B and SWF-C have the largest reversal magnetic fields at a wavelength of 642 and 681 nm, respectively. In the three

![Fig. 6 Simulated intensity of reversed magnetic field $H_y$ as a function wavelength (vertical coordinate) and sandwich diameter (i.e., transverse coordinate) for (a) SWF-A, (b) SWF-B, and (c) SWF-C. Thickness of SiO$_2$ film is 45 nm. (d) The inverse magnetic field $H_y$ in middle layer of SWF oscillating in a manner opposite to that of the applied magnetic field (blue region).](https://www.spiedigitallibrary.org/journals/Journal-of-Nanophotonics)
simulations, the average magnitude and area of the reversed magnetic field gradually decay as the thickness of SWF increases. Especially for the simulation of SWF-C, the area of the reversed magnetic field obviously shrinks obviously. Results of the FDTD simulation correlate with those of the detected spectra of permeability.

5 Conclusion

SWFs of various sizes are fabricated, along with their transmittance, reflectance, and absorptance compared as well. Although the absorptance increases with the SWF thickness, three samples with thicknesses of 420, 450, and 480 nm exhibit reflectance levels below 1%. The retrieved equivalent refractive index, forward impedance, and backward impedance reveal the propagation of the wave through SWF. Destructive interference for antireflection occurs even when the thickness of SWF is 480 nm. The dispersion of refractive index causes the low dispersion of optical thickness, resulting in destructive interference over the visible wavelengths. The decrease in measured negative equivalent permeability along with the thickness is interpreted qualitatively by simulating the reversed magnetic field at the center of each SWF. Simulation results indicate that the negative permeability arises from the reversal of the magnetic resonance within the SiO$_2$ layer. Furthermore, the reversed magnetic field becomes weaker as the thickness of Al increases, which corresponds to the trend of measured negative real part of the equivalent permeability.

Acknowledgments

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References

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