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Abstract. Stepped-chirp signal (SCS) is widely used by wideband high-resolution radars; however, its bandwidth synthesizing suffers from motion-induced phase errors resulting from the radial velocity of the target, especially for high-speed targets. So motion compensation is very crucial in signal processing for this kind of radar using SCS. Based on the cross-correlation inner frame method for velocity measurement of a single-scattering-center target, the multiple cross-correlation method (MCCM) is proposed for measuring the velocity of a complex target with multiple scattering centers (MSC), which is called SCS-MCCM. By this algorithm, not only the radial velocity, but also the real velocity of a target can be measured under the assumption that it is straight moving. After obtaining the velocity, motion compensation is conducted so as to realize high-resolution imaging. Theoretical analysis and simulations show that the proposed method is feasible and effective for an MSC target. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: [10.1117/1.JRS.8.083606](https://doi.org/10.1117/1.JRS.8.083606)]

Keywords: stepped-chirp signal; radar imaging; high-speed target; velocity measurement; motion compensation; stepped-chirp signal multiple cross-correlation method.

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1 Introduction

To meet the requirements of high-resolution range measurement or imaging, a step frequency technique has been proposed and has already become an important approach for modern radar systems. Stepped-chirp signal (SCS) has been a widely prevalent signal waveform used in synthetic aperture radar (SAR)/inverse SAR (ISAR).¹⁻³ However, there exists a severe range-Doppler coupling problem for SCS when applied to high-speed target imaging or detection. Because SCS is very sensitive to the radial velocity of target,⁴⁻⁷ the synthesized range profile suffers from range migration, energy diffusion, and resolution degradation, and even becomes meaningless if the motion compensation is not well done for high-speed target. So motion compensation is a crucial step in signal processing in this regard. There is a lot of research in this area and many methods for velocity measurement using SCS have been proposed, including the maximum likelihood method,^{8,9} iterative search method,¹⁰⁻¹² pulse-Doppler (PD) auxiliary method,¹³ up-down stepped-chirp method,¹⁴⁻¹⁶ cross-correlation between frames method,^{17,18} etc. However, each of the above-mentioned methods has its limitations, such as the maximum likelihood method and iterative search method need a large amount of computation, the PD auxiliary method and up-down stepped-chirp method need an additional transmitting signal besides SCS, the cross-correlation between frames method needs high pulse repeat frequency (PRF) to obtain high measurement accuracy, etc. Recently, a preferable method named the cross-correlation inner frame method (CCIFM) was proposed.¹⁹ It can measure the radial velocity of a high-speed target without using an auxiliary signal in a low PRF situation and has the advantages of a small amount of computation and a large unambiguous measurement range. Although the measurement accuracy is not the highest among these methods, it still satisfies the requirement for motion

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compensation. The outstanding disadvantage of CCIFM is that it is only suitable for a single-scattering-center (SSC) target. In this paper, we extend the idea of cross-correlation inner frame and propose a new velocity measurement method, which is named the SCS multiple cross-correlation method (SCS-MCCM). As will be shown later, the SCS-MCCM can keep the advantages of CCIFM while overcoming its disadvantages. It focuses on the velocity measurement for a high-speed target in a much more practical situation, i.e., the multiple-scattering-center (MSC) target is considered. In the following section, the property of correlations between two paired subpulses in the SCS burst is extensively investigated with detailed formulas derived. It is demonstrated that the instantaneous radial velocity information can be extracted from each echo burst. Simulations show that the proposed approach performs very well on radial velocity estimate for a high-speed MSC target. Based on the measured velocity, motion compensation is conducted and high-resolution imaging of a high-speed MSC target is realized. Besides the radial velocity, the real target velocity can also be measured by the SCS-MCCM, which is very helpful for target identification. This is another superiority of the SCS-MCCM compared to other methods.

2 CCIFM

The transmitted waveform consists of a series of chirp pulses (subchirps or subpulses), whose carrier frequencies increase (or decrease) pulse by pulse in a step of Δf . If the initial distance between radar and the target is R , the radial target velocity is V , and the pulse repeat interval is T_r , then the time delay of the i 'th subpulse is

$$\tau_i = \frac{2R}{c} - \frac{2iVT_r}{c}. \quad (1)$$

The echo of the i 'th subpulse after being coherently received is

$$s(t, i) = u(t, i) \exp \left[-j2\pi(f_0 + i\Delta f) \left(\frac{2R}{c} - \frac{2iVT_r}{c} \right) \right], \quad (2)$$

where $u(t, i) = \text{rect}[(t - \tau_i)/T_p] \exp[jK\pi(t - \tau_i)^2]$ is the baseband chirp pulse, f_0 is the carrier frequency of the first pulse, Δf is the frequency step, K is the slope of the subpulse, T_p is the subpulse time duration, $i = 0, 1, \dots, N-1$, and N is the number of subpulses in a burst. In the following, we ignore $u(t, i)$ because it has no significant role in the derivation, as will be shown in the following. After cross-correlation processing on two subpulses spaced by p subpulses, we can get

$$\begin{aligned} X(i) &= s(i) \cdot s^*(i+p) \\ &= \exp \left(-j2\pi f_0 p T_r \frac{2V}{c} \right) \exp \left(-j2\pi p^2 \Delta f T_r \frac{2V}{c} \right) \exp \left(j2\pi p \Delta f \frac{2R}{c} \right) \exp \left(-j2\pi 2p \Delta f \frac{2V}{c} i T_r \right), \\ i &= 0, 1, \dots, N-p, \quad 1 \leq p \leq N-1. \end{aligned} \quad (3)$$

Equation (3) shows that $X(i)$ contains four terms: the first three terms are constant phases and the last term is a linear item of i , which indicates a frequency shift. According to Eq. (3), the Doppler frequency of a moving target can be formulated as¹⁹

$$f_d = -2pT_r\Delta f \frac{2V}{c}, \quad (4)$$

which is proportional to V . So the target's velocity can be measured by fast Fourier transform (FFT) of $X(i)$. The velocity measurement accuracy is related to the resolution of Doppler frequency. If we increase the FFT dots to N_0 by zero-padding, the minimum measurable velocity is then

$$\Delta V = \frac{c}{4N_0pT_r\Delta f}, \quad (5)$$

while the velocity measurement scope is

$$V \in \left(-\frac{c}{8pT_r\Delta f}, \frac{c}{8pT_r\Delta f} \right). \quad (6)$$

Now, we shall show why $u(t, i)$ can be ignored in Eq. (3) in detail as follows. We can easily obtain the following expression:

$$\begin{aligned} u(t, i) \cdot u^*(t, i + p) &= \exp \left\{ jK\pi \left[t - \left(\frac{2R}{c} - \frac{2iVT_r}{c} \right) \right]^2 \right\} \exp \left(-jK\pi \left\{ t - \left[\frac{2R}{c} - \frac{2(i+p)VT_r}{c} \right] \right\}^2 \right) \\ &= \exp \left(-j\pi K \frac{4p^2 V^2 T_r^2}{c^2} \right) \exp \left(j\pi K \frac{8pVT_r}{c^2} R \right) \exp \left(-j2\pi t \frac{2pKVT_r}{c} \right) \exp \left(-j2\pi \frac{4pKV^2 T_r}{c^2} iT_r \right). \end{aligned} \quad (7)$$

For argument i , the first three terms in Eq. (7) are constant phases and the last term is a linear item, which indicates a frequency, i.e.,

$$f'_d = -\frac{4pKV^2 T_r^2}{c^2}. \quad (8)$$

Generally speaking, f'_d is much smaller than f_d , and the ratio $(f'_d/f_d) = (KVT_r/c\Delta f)$ is usually $<10^{-3}$, so it can be ignored.

3 SCS-MCCM

When the target is complex with MSCs, the correlation signals become much more complicated. Let us assume the number of scattering centers is M ; the echo of the i 'th subpulse is thus

$$s(t, i) = \sum_{m=1}^M \exp \left\{ jK\pi \left[t - \left(\frac{2R_m}{c} - \frac{2iVT_r}{c} \right) \right]^2 \right\} \exp \left[-j2\pi(f_0 + i\Delta f) \left(\frac{2R_m}{c} - \frac{2iVT_r}{c} \right) \right]. \quad (9)$$

Because $s(t, i)$ is the sum of echoes from M scatterers, the correlation signals will have self-terms (self-correlation of the same scatterer's echo) and cross-terms (cross-correlation of two different scatterers' echoes), which lead to different frequency shifts. Therefore, we cannot estimate the velocity just by FFT as is done in Sec. 2.

The cross-correlation between $s(t, i)$ and $s(t, i + p)$ is formulated as

$$\begin{aligned} X(t, i) &= s(t, i) \cdot s^*(t, i + p) \\ &= \sum_{m,n=1}^M \phi_1 \cdot \phi_2 \cdot \phi_3 \cdot \phi_4 \cdot \phi_5 \cdot \phi_6 \cdot \phi_7 \cdot \phi_8 \cdot \phi_9 \cdot \phi_{10} \cdot \phi_{11} \cdot \phi_{12} \cdot \phi_{13}, \end{aligned} \quad (10)$$

where

$$\begin{aligned}
\phi_1 &= \exp\left(-j2\pi f_0 p T_r \frac{2V}{c}\right) \\
\phi_2 &= \exp\left(-j2\pi p^2 \Delta f T_r \frac{2V}{c}\right) \\
\phi_3 &= \exp\left(-jK\pi \frac{4p^2 V^2 T_r^2}{c^2}\right) \\
\phi_4 &= \exp\left(-j2\pi \frac{2pKV T_r}{c} t\right) \\
\phi_5 &= \exp\left(j2\pi \frac{2K\Delta R_{m,n}}{c} t\right) \\
\phi_6 &= \exp\left(-j2\pi 2p\Delta f \frac{2V}{c} iT_r\right) \\
\phi_7 &= \exp\left(j2\pi \Delta f \frac{2\Delta R_{m,n}}{cT_r} iT_r\right) \\
\phi_8 &= \exp\left(-j2\pi \frac{4pKV^2 T_r}{c^2} iT_r\right) \\
\phi_9 &= \exp\left(j2\pi \frac{4KV\Delta R_{m,n}}{c^2} iT_r\right) \\
\phi_{10} &= \exp\left(-j\pi K \frac{4R_m^2 - 4R_n^2}{c^2}\right) \\
\phi_{11} &= \exp\left(j\pi K \frac{8pVT_r R_m}{c^2}\right) \\
\phi_{12} &= \exp\left(j2\pi p\Delta f \frac{2R_m}{c}\right) \\
\phi_{13} &= \exp\left(j2\pi f_0 \frac{2\Delta R_{m,n}}{c}\right) \\
\Delta R_{m,n} &= R_m - R_n, 1
\end{aligned}$$

Among the above phase terms, ϕ_1 , ϕ_2 , and ϕ_3 are constant phases, ϕ_{10} , ϕ_{11} , ϕ_{12} , and ϕ_{13} are constant phases related to R , ϕ_4 and ϕ_5 are linear items about t , and ϕ_6 , ϕ_7 , ϕ_8 , and ϕ_9 are linear items about i . As is shown, there are no coupling items about t and i .

So, $X(t, i)$ has M^2 terms, including M self-terms (when $m = n$) and $M(M - 1)$ cross-terms (when $m \neq n$), which have different linear coefficients. That means the two-dimensional (2-D) spectrum of $X(t, i)$ has many frequency components, and each of them corresponds to a self-term or a cross-term of $X(t, i)$.

For self-terms, ϕ_5 , ϕ_7 , ϕ_9 , ϕ_{10} , and ϕ_{13} do not exist. As ϕ_8 is very small, as has been discussed previously, it can be ignored. With the constant phases ϕ_1 , ϕ_2 , and ϕ_3 further ignored, we get

$$X(t, i)_{\text{self}} = \phi_4 \cdot \phi_6 \sum_{m=1}^M \phi_{11} \cdot \phi_{12}. \quad (11)$$

$$X(t, i)_{\text{cross}} = \phi_4 \cdot \phi_6 \sum_{m,n=1, m \neq n}^M \phi_5 \cdot (\phi_7 \cdot \phi_9) \cdot (\phi_{10} \cdot \phi_{11} \cdot \phi_{12} \cdot \phi_{13}). \quad (12)$$

Let f_t represent the frequency along the t direction and f_d represent the frequency along the i direction. Because ϕ_4 (the linear item about t) and ϕ_6 (the linear item about i) are not related to the scatterer's position R_m , f_t and f_d of the M self-terms should be the same, and they are denoted as f_t^0 and f_d^0 , respectively.

$$f_t^0 = -\frac{2pKV T_r}{c}, \quad (13)$$

$$f_d^0 = -2p\Delta f \frac{2V}{c} \quad (14)$$

The $M(M-1)$ cross-terms have different f_t and different f_d , which are related to the relative positions of scattering centers $\Delta R_{m,n}$. As shown in Eq. (12), f_t is decided by ϕ_4 and ϕ_5 , and f_d is decided by ϕ_6 , ϕ_7 , and ϕ_9 , i.e.,

$$f_t = f_t^0 + \frac{2K\Delta R_{m,n}}{c} \triangleq f_t^0 + f_t^1, \quad (15)$$

$$f_d = f_d^0 + \Delta f \frac{2\Delta R_{m,n}}{cT_r} + \frac{4KV\Delta R_{m,n}}{c^2} \triangleq f_d^0 + f_d^1. \quad (16)$$

From Eqs. (15) and (16), we can see that f_t and f_d are symmetrical pairs about f_t^0 and f_d^0 , respectively.

When f_d^1 is less than a frequency resolution cell, i.e., $|f_d^1| < [1/(T_r \cdot N_0)]$, we can have $f_d \approx f_d^0$. In this situation, the target can be regarded as a point target, so the velocity can be measured using the algorithm mentioned in Sec. 2. It means that the size of target should meet the requirement of $|\Delta R_{m,n}| < [c/(2\Delta f N_0)]$, which is usually not satisfied in practical situations. That is to say the performance of the algorithm of Sec. 2 cannot be as good as we expect for bigger targets.

In fact, we can also see from Eqs. (15) and (16) that the frequencies of cross-terms f_t and f_d are determined not only by V , but also by $\Delta R_{m,n}$. However, from Eqs. (13) and (14), we can see that the frequencies of self-terms f_t^0 and f_d^0 are determined only by V . Therefore, if we can differentiate them in the 2-D spectrum of $X(t, i)$, the velocity can then be estimated by f_t^0 and f_d^0 .

If a signal is sampled at rate f_s and the sampling length is L , then the resolution of the spectrum is f_s/L . When $|f_t^1| > f_s/L$, i.e., the distances between scattering centers of the target satisfy the following condition:

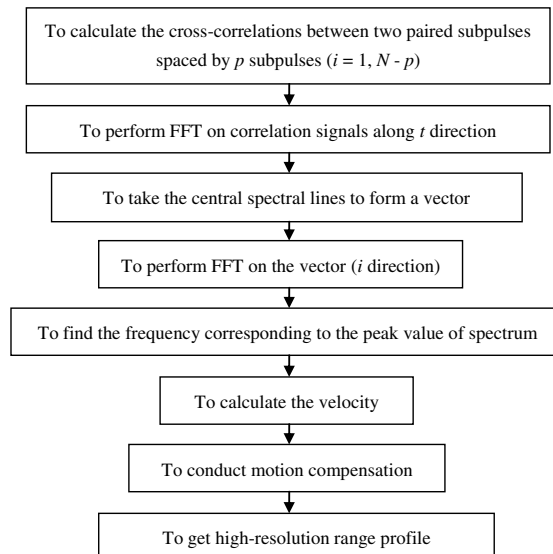


Fig. 1 The flow chart of stepped-chirp signal multiple cross-correlation method (MCCM).

$$|\Delta R_{m,n}| > \frac{cf_s}{2KL}, \quad 1 < m, n < M. \quad (17)$$

After performing FFT on $X(t, i)$ along the t direction, f_t and f_t^0 will be at least one frequency cell apart, so they can be easily distinguished. In fact, Eq. (17) is easy to meet via increasing L by interpolation. Since f_t is symmetrically distributed around f_t^0 , we can just choose the central frequency of the spectrum to get rid of all other frequency components of the cross-terms. At the last step, we get f_d^0 by conducting FFT along the i direction and, finally, obtain the velocity by

$$\hat{V} = -\frac{c}{4p\Delta f} f_d^0, \quad (18)$$

where $p \in [1, N-1]$. It is clear from Eq. (18) that the larger the p , the higher the measurement accuracy but the less the unambiguous measurement range of velocity. We must choose an appropriate p to balance the measurement range and accuracy. In fact, we can use a smaller p to conduct a coarse measurement with a large unambiguous range first and then use a larger p to conduct an accurate measurement.

Figure 1 presents the flow chart of the proposed method, including the motion compensation step. The first step is to calculate a series of cross-correlations between two paired subpulses spaced by p subpulses ($i = 1, N-p$); the second step is to perform FFT on the correlation signals along the t direction for $i = 1, N-p$; the third step is to take the central spectral line of each pair to form a vector; the fourth step is to perform FFT on the above vector; the fifth step is to find the frequency corresponding to the peak value of the spectrum; the sixth step is to calculate the radial velocity according to Eq. (18); the seventh step is to conduct motion compensation according to the obtained velocity; the last step is to coherently synthesize the spectrums of all subpulses using the algorithm of Ref. 20 and, finally, get the high-resolution range profile through Inverse FFT (IFFT).

4 Real Velocity Measurement

In this section, we shall show that besides the radial velocity, SCS-MCCM can also be used to measure the real velocity of the target. SCS-MCCM measures the radial velocity from the echoes of subpulses within a burst, i.e., it measures the instantaneous radial velocity at each burst. Then the real velocity can be estimated by combining the radial velocity measurement with the range measurement. Here, the target is supposed to be well tracked by radar.

We assume that the target moves straight during the observation time, as shown in Fig. 2. The real target velocity is V_0 . When the radar is transmitting the j 'th burst ($j = 1, 2, 3, \dots$), the distance between radar and target is R_j , and the angle between the target moving direction and radar boresight is θ_j , so the radial velocity is $V_j = V_0 \cos \theta_j$ (V_j is positive when $\theta_j < 90^\circ$ and negative when $\theta_j > 90^\circ$).

If the burst repeat interval is T_b , then the distance between target position 1 and target position j is $V_0(j-1)T_b$. According to the cosine law, we can get Eqs. (19) and (20), respectively, as follows:

$$\cos \theta_1 = \frac{R_1^2 + [V_0(j-1)T_b]^2 - R_j^2}{2R_1V_0(j-1)T_b}, \quad (19)$$

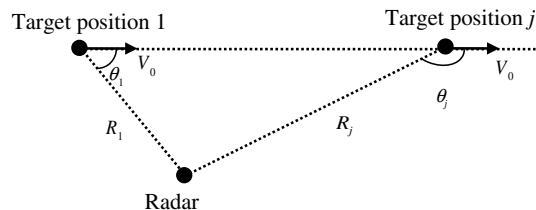


Fig. 2 The observation geometry.

$$\cos(\pi - \theta_j) = \frac{R_j^2 + [V_0(j-1)T_b]^2 - R_1^2}{2R_jV_0(j-1)T_b}. \quad (20)$$

By substituting $\cos \theta_1 = (V_1/V_0)$ into Eq. (19), we can get

$$R_j^2 - R_1^2 = [V_0(j-1)T_b]^2 - 2R_1V_1(j-1)T_b. \quad (21)$$

By substituting $\cos(\pi - \theta_j) = -(V_j/V_0)$ into Eq. (20), we can get

$$R_j^2 - R_1^2 = -2R_jV_j(j-1)T_b - [V_0(j-1)T_b]^2. \quad (22)$$

Finally, V_0 can be derived simultaneously from Eqs. (21) and (22).

$$V_0 = \sqrt{\frac{R_1V_1 - R_jV_j}{(j-1)T_b}}. \quad (23)$$

Equation (23) indicates that the real velocity measurement can be easily obtained by using the results of the range measurement as well as the radial velocity measurement, where the range measurement can be done according to the time delay of the radar echoes.

In the following, let us analyze the impact of measurement errors of R_j and V_j on V_0 estimation. The measurement error (or accuracy) of V_0 , i.e., ΔV_0 , can be formulated as follows:

$$\Delta V_0 = \sqrt{\left(\frac{\partial V_0}{\partial R_j} \Delta R_j\right)^2 + \left(\frac{\partial V_0}{\partial V_j} \Delta V_j\right)^2}, \quad (24)$$

where ΔR_j and ΔV_j are the measurement errors of R_j and V_j , respectively. Equation (24) shows that when ΔR_j and ΔV_j are fixed (as discussed above), the smaller the partial derivatives with respect to R_j and V_j , the smaller the measurement error of V_0 , i.e., the higher the measurement accuracy of V_0 .

The partial derivatives of Eq. (23) with respect to R_j and V_j , respectively, are as follows:

$$\frac{\partial V_0}{\partial R_j} = -\frac{V_j}{2\sqrt{(R_1V_1 - R_jV_j)(j-1)T_b}}, \quad (25)$$

$$\frac{\partial V_0}{\partial V_j} = -\frac{R_j}{2\sqrt{(R_1V_1 - R_jV_j)(j-1)T_b}}. \quad (26)$$

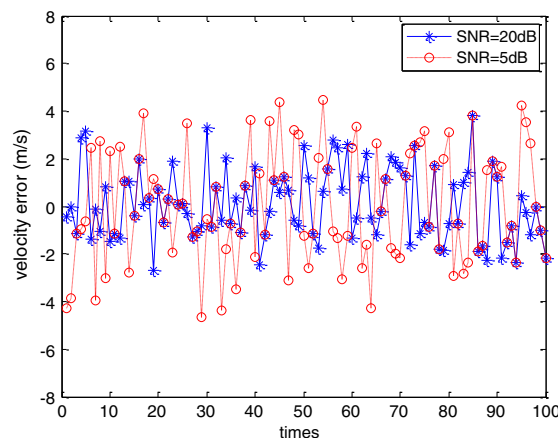


Fig. 3 The velocity measurement errors for single-scattering-center (SSC) target.

In Eqs. (25) and (26), when $\theta_j < 90^\circ$, V_j is positive. Along with the increase in j , $(j-1)T_b$ becomes larger, while V_j and R_j become smaller, so $(R_1V_1 - R_jV_j)$ is positive and becomes larger, too; thus, the absolute values of $\partial V_0/\partial R_j$ and $\partial V_0/\partial V_j$ both become smaller. When $\theta_j > 90^\circ$, V_j is negative, and its absolute value becomes larger as j increases. Along with increase in j , $(j-1)T_b$ and R_j also become larger, so $(R_1V_1 - R_jV_j)$ is still positive and becomes larger, too; once again, the absolute values of $\partial V_0/\partial R_j$ and $\partial V_0/\partial V_j$ both become smaller.

From the above analysis, we observed that the larger the j , the smaller $\partial V_0/\partial R_j$ and $\partial V_0/\partial V_j$. Therefore, in order to achieve high measurement accuracy of V_0 , we should choose a j as large as possible.

5 Simulations

The simulation parameters are as follows: $f_0 = 13$ GHz, $\Delta f = 100$ MHz, $B = 120$ MHz, $T_r = 16$ μ s, $N = 20$, $p = 6$. Monte-Carlo simulations are conducted 100 times when the target velocities are produced with a uniform distribution in (5000 m/s, 5500 m/s). For the SSC target, CCIFM and SCS-MCCM have the same performance for the velocity measurement. Figure 3 presents the error curves of the velocity measurements for the SSC target with different SNRs. Results show that in the case of SNR = 20 dB, the maximum measurement error is <4 m/s, while in the case of SNR = 5 dB, the maximum measurement error is <5 m/s. That is to say the measurement error does not change significantly as the SNR decreases, i.e., MCCM exhibits a satisfied antinoise performance for the SSC target.

Figures 4(a) and 4(b) present the high-resolution range profiles without and with motion compensation, respectively. When the target is moving at a high speed, the motion-induced phase errors will lead to image displacement and the image will be out of focus; therefore, high resolution cannot be achieved, as clearly shown in Fig. 4(a). Figure 4(b) shows that after velocity measurement and motion compensation, the burst of stepped-chirp can be synthesized correctly and a high-resolution range profile is, thus, obtained. The resolution in Fig. 4(b) is ~ 0.075 m, which is close to the theoretical value of a 2.04-GHz bandwidth signal. In the following, we shall demonstrate the good performance of the SCS-MCCM for an MSC target. Figure 5 gives the MSC target model used for the velocity measurement and imaging simulations, which is composed of 41 ideal point targets.

We conduct Monte-Carlo simulation 100 times as before for the MSC target of Fig. 5 by using CCIFM with an SNR = 20 dB and plot the obtained velocity measurement errors in Fig. 6, from which one can clearly see that they are very large and fluctuate dramatically. It means that CCIFM breaks down for the MSC target velocity measurement. Figure 7 presents the error curves of the velocity measurement by SCS-MCCM for the same MSC target with different SNRs. The target velocities in Figs. 7(a), 7(b), and 7(c) are varied in the range of (2000 m/s, 2500 m/s), (5000 m/s, 5500 m/s), and (7000 m/s, 7500 m/s), respectively.

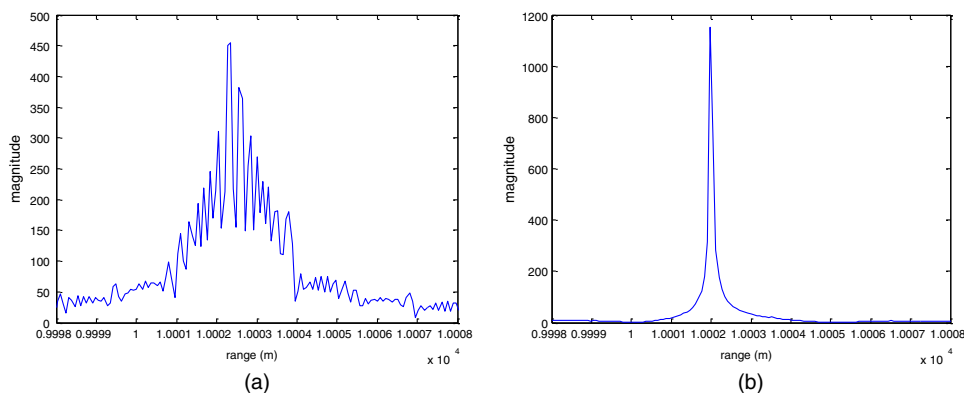


Fig. 4 The synthesized range profiles for SSC target (a) without motion compensation and (b) with motion compensation.

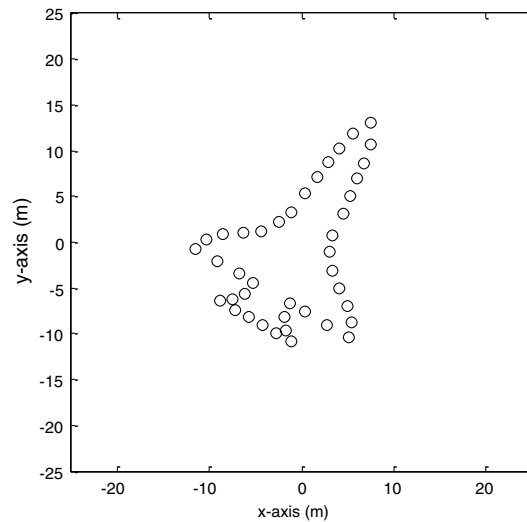


Fig. 5 The multiple scattering centers (MSC) target model.

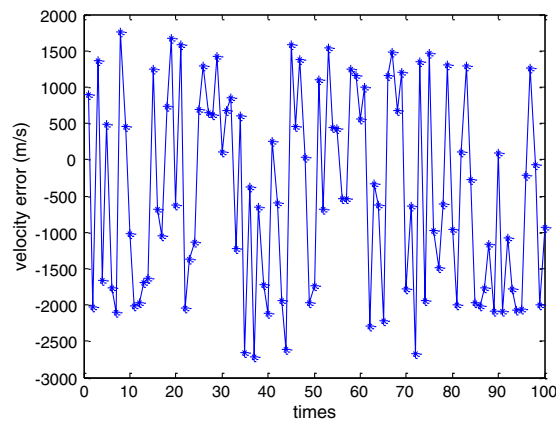


Fig. 6 The velocity measurement error of cross-correlation inner frame method (CCIFM) for MSC target (SNR = 20 dB).

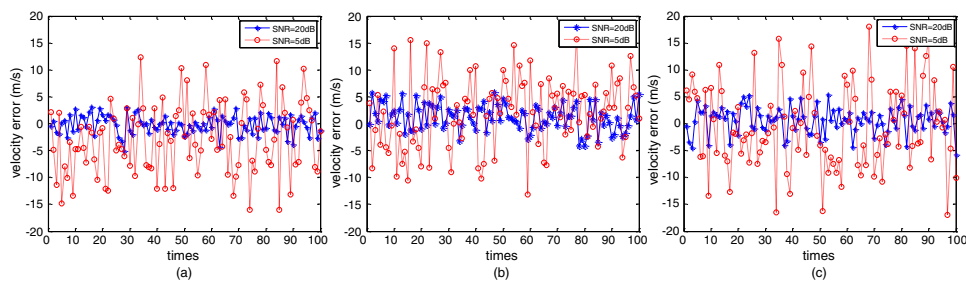


Fig. 7 The velocity measurement errors of MCCM for MSC target: (a) $V \in (2000 \text{ m/s}, 2500 \text{ m/s})$, (b) $V \in (5000 \text{ m/s}, 5500 \text{ m/s})$, and (c) $V \in (7000 \text{ m/s}, 7500 \text{ m/s})$.

We can see from Fig. 7 that the measurement errors of the SCS-MCCM do not change as the target velocity changes, and they are all within 6 m/s when SNR = 20 dB, while the maximum measurement errors are ~ 17 m/s when SNR = 5 dB. Compared to the SSC target case, the measurement accuracy for the MSC target degrades remarkably as the SNR decreases. It means the performance is more sensitive to SNR. However, the accuracy still satisfies the requirement for motion compensation processing. Berizzi and Martorella derived the velocity accuracy requirement for SCS signal motion compensation¹² as $\Delta V < [c/(4Nf_0T_r)]$, i.e., it is ~ 18 m/s with the parameters of this paper.

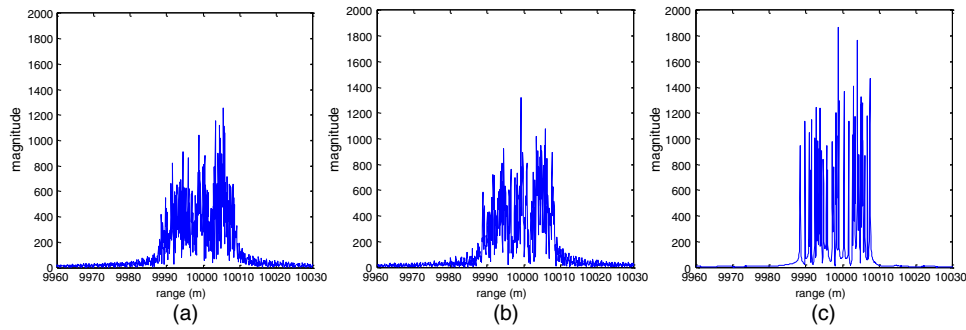


Fig. 8 The synthesized range profiles for MSC target (a) without motion compensation and (b) with motion compensation using CCIFM, and (c) with motion compensation using MCCM.

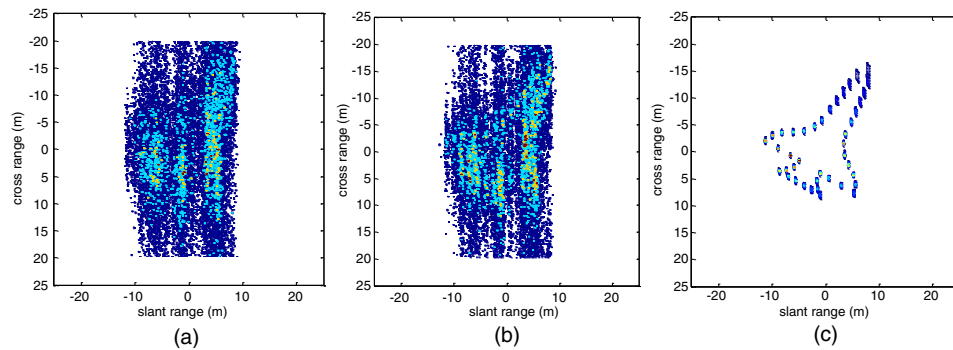


Fig. 9 The imaging results (a) without motion compensation and (b) with motion compensation using CCIFM, and (c) with motion compensation using MCCM.

Figures 8 and 9 present the stepped frequency radar imaging results for the target of Fig. 5 using the system parameters as listed in Table 1 under the geometry of Fig. 2, where the initial distance R_1 between the radar and the target is 10 km, the initial view angle $\theta_1 = 60^\circ$, and the real target velocity $V_0 = 7000$ m/s.

Figure 8(a) presents the synthesized range profile without motion compensation, from which one can see that the high-speed motion-induced phase errors make the range profile seriously smear. Figure 8(b) shows the result with motion compensation conducted using CCIFM. Because CCIFM cannot correctly measure the velocity of the MSC target, Fig. 8(b) scarcely improves compared to Fig. 8(a). Figure 8(c) gives the synthesized range profile with motion compensation conducted using SCS-MCCM; it is very well profiled as we expected. Figure 9(a) shows the 2-D imaging result without motion compensation. Due to the high

Table 1 Simulation parameters.

Initial carrier frequency	13 GHz
Frequency step	100 MHz
Bandwidth	120 MHz
Number of pulses	20
Pulse width	8 μ s
Subpulse repetition interval	16 μ s
Burst repetition interval	2 ms
Number of burst	128
SNR	20 dB

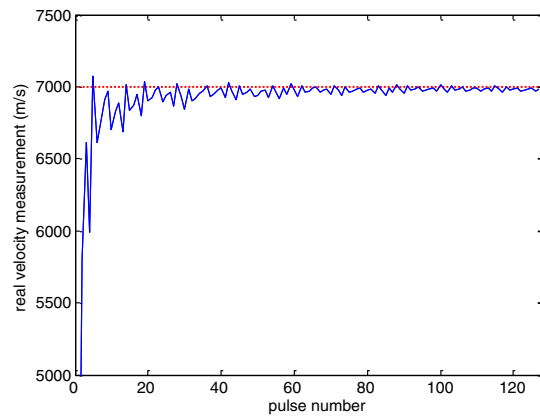


Fig. 10 The real velocity measurement for SSC target.

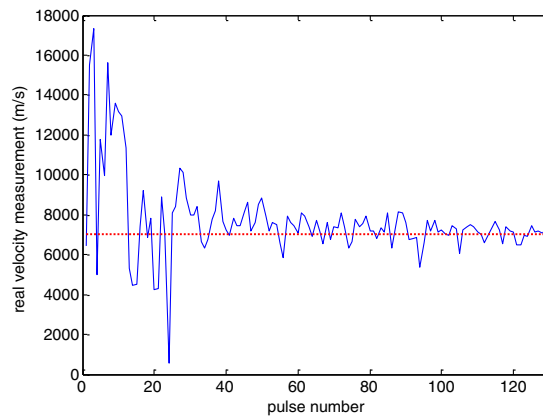


Fig. 11 The real velocity measurement for MSC target.

speed of the target, the motion-induced phase errors make the image seriously blurred. Figures 9(b) and 9(c) are the images with motion compensation conducted using CCIFM and SCS-MCCM, respectively. As before, one can see that CCIFM does not work in the MSC target case. However, SCS-MCCM can handle this case and the radar image is very well focused, as shown in Fig. 9(c). The results of Fig. 9 also indicate that the high-speed motion-induced errors affect not only the range profiles, but also azimuth focusing. The above simulation experiments demonstrate that the proposed velocity measurement method for a high-speed target based on SCS is valid and effective, and the resulting measurement error can meet the requirement for high-resolution imaging.

Figures 10 and 11 present the real velocity measurement results using the same parameters and geometry as in the previous imaging simulation. The solid curves represent the estimated values versus the used number of received pulses. The dotted lines represent the real velocity set in the simulation, which is 7000 m/s. From these two figures, one can see that the curves fluctuate severely and the measurement errors are quite large for both SSC and MSC targets when only several pulses are received and used. With an increase in the number of received pulses, the fluctuations of the curves quickly reduce, and the estimated values gradually approach the true value. The variance of the curve in Fig. 11 is larger than that in Fig. 10 because the velocity measurement accuracy for the SSC target is better than that for the MSC target. If we just take into account the parts of curves with a pulse number > 64 , we get the mean values of 6981 m/s in Fig. 10 and 7147 m/s in Fig. 11, respectively, i.e., the relative measurement errors are ~ 0.27 and 2.1% , respectively.

6 Conclusion

High-resolution radar imaging of a high-speed target using SCS must properly solve the problem of motion estimation and compensation. We propose the SCS-MCCM to accurately measure the

velocity of a high-speed target with MSCs, which is the first step for high-resolution imaging. Detailed analysis and derivations of the proposed method are presented. Although it is not the most accurate method of velocity measurement with SCS, the advantages of SCS-MCCM make it practically applicable and easy to adopt. It can measure the target radial velocity by using only the echoes of subpulses within a burst, so it does not require a high repetition frequency of burst and, thus, has a large unambiguous measurement range. If the target moves straight, this method can also be used to measure the real velocity of the target. To show the validation and effectiveness of the method, simulations for an MSC target are conducted, which clearly show that the radar image is very well focused after performing motion compensation using the proposed method, but is not focused by using CCIFM; at the same time, the real target velocity is also well estimated. We should emphasize that there is still a room for improving the velocity measurement accuracy for an MSC target with the proposed method, and this is our next effort.

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