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Abstract. The performance of a multibeam laser system is evaluated for coherent and incoherent beam combination under tactical scenarios. For direct comparison, identical aperture geometries are used for both coherent or incoherent, combination methods. The analysis assumes a multilaser source coupled with a conventional 0.32 m diameter, on-axis, beam director. Parametric analysis includes variations over residual errors, beam quality, atmospheric effects, and scenario geometry. Analytical solutions from previous results are used to evaluate performance for the vacuum case, providing an upper bound on performance and a backdrop for organizing the multitude of effects as they are analyzed. Wave optics simulations are used for total system performance. Each laser in the array has a wavelength of 1.07 μm, 10 kW (25 kW) output power, and Gaussian exitance profile. Both tracking and full-aperture adaptive optics are modeled. Three tactical engagement geometries, air to surface, surface to air, and surface to surface, are evaluated for slant ranges from 2.5 to 10 km. Two near-median atmospheric profiles were selected based upon worldwide climatological data. The performance metric used is beam propagation efficiency for circular target diameters of 5 and 10 cm. © 2012 SPIE

1 Introduction

Waveguide laser technology has rapidly advanced in the past decade and has garnered favor over chemical laser sources for future directed energy (DE) applications. Waveguide lasers include both fiber lasers and planar waveguide lasers. The first, fiber lasers, has received abundant attention as a possible replacement for a chemical device. Fiber lasers have the beneficial features of long lifetimes, high efficiency, and high beam quality. A single mode fiber laser can now provide multiple kilowatts of power at wall plug efficiencies >25%. The weight-to-power ratio for fiber lasers is approaching that of chemical devices. But, at 10 kW per fiber, multiple sources must be combined to achieve useful power levels for tactical applications. Since fiber lasers at these power levels have too broad of an optical bandwidth for practical phasing, multiple sources would be used in a power adding architecture, also called incoherent beam combining (IBC). In contrast, narrow bandwidth, single-mode fiber lasers are currently limited to power levels below 1 kilowatt, else nonlinear effects dominate and destroy performance. Coherent phasing of narrowband fiber lasers has been demonstrated for 32 fiber lasers with residual phase errors less than λ/70 root-mean-squared (RMS). Even though no apparent limit exists for coherent beam combining (CBC) hundreds of narrow band fiber sources, the risk due to practicalities of such a system must be considered high.

Another waveguide laser type, the planar waveguide laser, such as that being researched by Raytheon, shares many of the advantages of fiber lasers and is showing promise in meeting power levels >10 kW levels with narrow line widths of <10 MHz. With these new developments in narrow band, kW-power sources, it is possible to consider the design tradeoffs between identical projecting apertures for both coherent and incoherent beam combining of multiple sources for use in a tactical DE system. Previous articles have considered such topics, but their designs used different aperture geometries for the coherent and the incoherent cases. Comparing performance over different aperture geometries is both limited in scope and difficult to apply in general. This work starts by defining identical aperture geometries and power levels for both CBC and IBC, and provides detailed analysis to develop a fundamental understanding of the various tradeoffs between the two combination methods.

The remainder of the paper begins with a definition of a design that is amenable for either CBC or IBC. Theoretical analysis is presented that can model either CBC or IBC of the proposed aperture geometry with the proper choice of piston variation between the pupil subapertures. Numerical methods are used to analyze the effects of subaperture piston and tilt errors on performance, as well as the effects of beam profile, target size, fill factor, and aperture geometry. Since the
design uses a single tracker to point the aperture, the effects of pupil mismatch first presented by Fried and Greenwood, are evaluated. Wave optics simulations allow for a complete evaluation of sensitivity and combined effects, including beam quality, platform jitter, adaptive optics, and thermal blooming. The wave optics simulations use a median-atmosphere for absorption and scattering levels with two turbulence levels. The impact of turbulence distribution on performance is included by defining and analyzing performance over three tactical engagement geometries. The paper concludes with a summary of performance of a system with nominal values for all parameters which are considered achievable with current technology. In general, it is shown that CBC always outperforms IBC for tactical engagements with a minor exception. This exception is discussed in detail throughout the paper. The paper provides sufficient comparison of the two methods to show the performance-benefit trade-off of coherent combination over incoherent combination.

2 Background

A typical, tactical architecture for the comparative evaluation of the key design issues for coherent beam combining (CBC) and incoherent beam combining (IBC) is shown in Fig. 1. Fan surveys current methods under study for beam combining. Possible combination methods of multiple laser sources vary, but those methods applicable for tactical power levels can all be classified as either coherent or incoherent. All proposed beam combination methods can be readily adapted to an architecture that uses a single beam director, i.e., a gimbaled telescope, for beam projection. The architecture shown in Fig. 1 is considered the most practical and cost effective for the capabilities required to project a multilaser source in the case of either coherent or incoherent beam combining. This architecture allows for a direct comparison of coherent and incoherent combination without requiring new invention and its associated complexity. The beam director both transmits and receives allowing for proven solutions to pointing, tracking, and adaptive optics. Essentially, this architecture is an incremental change to any previously proposed DE tactical systems that would use a single source, but the design in this work presumes a multilaser source. Other approaches for IBC have proposed individual trackers, adaptive optics, and beam directors as a possible architecture. The analysis within this paper is general enough to include this approach. The on-axis beam expander precludes a subaperture source on axis and, thus, reduces the fill factor (later defined in detail) leading to a reduction in propagation efficiency (also, defined shortly). However, the architecture is proposed as a design increment towards an optical phased array system which requires coherent transmitting and receiving through individual beam directors for each source element. In this respect, the paper concentrates only on the use of multilaser sources and directly compares the performance metric of propagation efficiency for the cases of incoherent and coherent beam combining. Less ambitious than an optical phased array system, this architecture has the advantage of lower cost with less technology development required for such a system and provides an intermediate look at the issues and advantages of phasing the source.

An IBC methodology that optically overlays multiple sources with spectral combining, polarized beam splitters, or dichroic beam splitters, provides a full beam at the pupil of the transmitter indistinguishable from that of single source with the same total power. The analysis of propagation performance of this IBC system is equivalent to that of a single beam source, and as such, is not addressed here. The remaining beam combining approaches can all be accommodated efficiently into the architecture of Fig. 1. More importantly, the analysis within provides a direct comparison of CBC and IBC with identical transmitting architectures, i.e., the geometry in the pupil is unchanged in comparison. This distinction separates this paper from previous references (see Refs. 2 and 5). The performance measure, propagation efficiency, is the ensemble averaged, integrated power over standard target sizes normalized by the power in the exit pupil of the transmitter. This metric is identical to previously published analysis and links the results directly for independent, follow-on lethality analysis.

The system design analyzed in this paper consists of a traditional 0.32 m diameter, on-axis beam director with a 20% central obscuration, where the monolithic laser is replaced by six tiled lasers, also referred to as subapertures (see Fig. 1). The subapertures are arranged in a hexagonal pattern with expanded dimensions of 10 cm diameter, d, at the exit pupil of the beam director and 11 cm center-to-center separation, ‘s.’ Each subaperture projects a 10 kW laser beam that is spatially coherent. The subaperture beams are collimated before the beam director and focused on target with the monolithic telescope optics of the beam director. The analysis assumes that coherent combining occurs in compact space (before beam expansion), but does not consider any specific method for phasing in detail nor phasing on target. Rather, the analysis parameterizes phasing performance by including residual beamlet tilt and piston errors for each subaperture.

Considerable research is currently addressing coherent combination to achieve tactical power levels as a viable alternative to a single, solid state source. Coherent combination increases the peak irradiance proportional to N^2 by phase matching the output of each source, were as, incoherent combining gives an irradiance that is linear in the number of apertures. The additional complexity in phasing the

Fig. 1 Conceptual layout of a multilaser source with an on-axis beam director. This example considers a six-element source, each at 10 kW (60 kW) of power. As annotated, this architecture lends itself to a single tracker and possible adaptive optics system. Note that this layout, while allowing direct comparison of CBC and IBC, produces a relatively low fill factor. The aperture sharing element (ASE) combines the tracker and wavefront sensor (WFS) lines-of-sight before the deformable mirror (DM).
sources merits analysis that addresses the tradeoff between coherent and incoherent performance.

2.1 Description of Scenarios

The analysis uses three typical, tactical scenarios for evaluating CBC and IBC. The turbulence being stronger near the surface impacts performance depending on the scenario geometry. The scenarios use the generic names: air-to-surface (A2S), surface-to-air (S2A), and surface-to-surface (S2S). The description of each, listed in Table 1, provides enough information to perform the paper’s detailed analysis and to relate each to an individual service’s tactical engagement. A2S represents an airborne laser moving toward and firing upon a stationary ground target. S2A is the reciprocal of A2S, and represents a stationary ground laser firing at an aircraft. S2S represents a ship-to-ship horizontal path engagement. The complete design space, used in conjunction with the scenario definitions found in Table 1, is listed in Table 2. The analysis to follow will vary the parameters listed in Table 1 individually and in combinations, to show the effects on performance. Here, we provide a complete listing for convenient reference.

3 Beam Combination Theory

The theory presented in this paper is based on work published by Butts. Butts’ development concentrates on Strehl performance of a phased array of coherent sources for various levels of subaperture piston and tilt disturbances. This paper uses the metric of beam propagation efficiency (BPE) which is the ensemble averaged, integrated power in a circular bucket in the target plane normalized by the total power in the exit pupil. This metric emphasizes the important system performance of energy coupling to the target and avoids esoteric nuances, such as irradiance profiles on target, not considered necessary in a comparative study. BPE is closely related to power in the bucket (PIB), but generalizes the concept as a neutral metric when comparing coherent and incoherent combining. Other common metrics, such as $M^2$ and Strehl ratio do not accurately describe the performance of coherently combined lasers. The analysis considers two bucket sizes, a 5 cm diameter and a 10 cm diameter circular bucket. These sizes represent typical target sizes for a tactical laser weapon.

3.1 Subaperture Piston and Tilt Errors

The focused irradiance pattern at the target plane is developed by modeling a coherent array with each subaperture field being uniform and containing terms to account for subaperture tilt and piston. The modulus squared of the combined fields can then model either a coherent array, by using little or no piston variations, or an incoherent array by choosing a high enough piston variation. The analysis assumes that the tilt and piston variations are equal in magnitude and pair-wise independent. This is reproduced from Butts.

Define a uniform field across each individual subaperture as

$$U_n(\vec{r}_1) = (P/A)^{1/2} \exp\{i\vec{k}[a_n + b_n(x_1 - \bar{x}_n)] + c_n(y_1 - \bar{y}_n)]\}.$$  \hspace{1cm} (1)

where $U_n(\vec{r}_1)$ is the field over the $n$th subaperture centered at $(\bar{x}_n, \bar{y}_n)$, $P$ is the power in the $n$th subaperture, $A$ area of a single subaperture, $k$ propagation vector with magnitude $2\pi/\lambda$; where $a_n$, $b_n$, and $c_n$ are independent Gaussian random variables, $a_n$ is the piston over the $n$th-subaperture; $b_n$ and $c_n$ are the x- and y-tilt, respectively, over the $n$th-subaperture, $(a_n^2) = \sigma_a^2$ and $(b_n^2) = (c_n^2) = \sigma_T^2$ with the angle brackets signifying ensemble averaging.

The total focused field of the array in the target plane (neglecting leading phase terms) is then

$$U(\vec{r}, z) \approx \int_A U_n(\vec{r}_1) \exp(-ik \cdot \vec{r}_1/z)d^2\vec{r}_1.$$  \hspace{1cm} (2)

The ensemble averaged, focused, far field irradiance is calculated in Ref. as

\begin{table}[h]
\centering
\caption{Tactical scenario details.}
\begin{tabular}{lll}
\hline
Engagement & Parameter & Value \\
\hline
Air to surface & Slant range & 2.5, 5, 7.5, and 10 km \\
 & Platform altitude & 1524 m \\
 & Platform speed & 100 m/s \\
 & Platform heading & 000 deg \\
 & Target altitude & 3 m \\
 & Target speed & 0 m/s \\
 & Target heading & 180 deg \\
Surface to air & Slant range & 2.5, 5, 7.5, and 10 km \\
 & Platform altitude & 3 m \\
 & Platform speed & 0 m/s \\
 & Platform heading & 000 deg \\
 & Target altitude & 1524 m \\
 & Target speed & 100 m/s \\
 & Target heading & 180 deg \\
Surface to surface & Slant range & 2.5, 5, 7.5, and 10 km \\
 & Platform altitude & 15 m \\
 & Platform speed & 0 m/s \\
 & Platform heading & 000 deg \\
 & Target altitude & 15 m \\
 & Target speed & 10 m/s \\
 & Target heading & 270 deg \\
\hline
\end{tabular}
\end{table}
\[ I(\bar{r}, z) = \left( \frac{P}{\lambda^2 z^2 A} \right) \left\{ 4\pi d^2 \int_0^1 \rho d\rho \exp \left\{ -k^2 \sigma_p^2 d^2 \rho^2 / 2 \right\} \right. \]
\[ \times \left. \left[ \cos^{-1}(\rho) - \rho \sqrt{1 - \rho^2} J_0(kd\rho/z) \right] \right. \]
\[ + 4\pi^2 \exp(-k^2 \sigma_p^2) \sum_{n,m} \exp(-ik\bar{r} \cdot (\bar{r}_n - \bar{r}_m)/z) \]
\[ \times \left[ \int_0^{d/2} r_1 d r_1 \exp \left\{ -k^2 \sigma_T^2 \sigma_p^2 / 2 \right\} \right. J_0(krr_1/z) \right. \]
\[ \left. \left. \right\}^2 \right. \]
\[ (3) \]

where \( J_0 \) is a Bessel function of the first kind and all other terms have been defined previously, \( d \) is the diameter of a subaperture, \( r_a \) is the vector location of the center of the \( n \)th subaperture, \( r \) is the radial distance in the far field; and \( z \) is the distance to the far field pattern.

This analytical formulation provides an envelope of performance that provides intuition before proceeding to a wave optics simulation. A plot of BPE using Eq. (3) is instructive in understanding the tradeoffs between coherent and incoherent combining for the same pupil geometry. Figure \[ 2(a) \] is a 3D plot of BPE for a 5 cm circular bucket with the beam focused at 7.5 km. The independent axes show the effect due to increases in subaperture RMS tilt jitter and subaperture RMS piston jitter as defined in Eq. (3), \( \sigma_T, \sigma_p \), respectively. The plot on the top right [Fig. 2(b)] is for the case of subaperture tilt jitter only, while the plot on the bottom right [Fig. 2(c)] is for subaperture piston jitter only. Considering each effect individually, BPE approaches zero as subaperture tilt RMS is increased, yet the increase in piston RMS only shows that BPE asymptotes to the \( n \)-subaperture incoherent performance (IBC). The latter is intuitively pleasing since we would expect the subaperture beamlets to be completely incoherent with each other when the RMS disturbance approaches that for a uniform, random distribution over \( \pm \pi \). The analytical model of the array for the range of 7.5 km and a 5 cm bucket shows CBC provides more energy on target than IBC. The assumption that this is strictly true for all ranges and bucket sizes though is not correct and leads to a key design tradeoff for a multiaperture system. This topic is addressed in detail in the subsequent sections.

### 3.2 Comparison of Uniform and Truncated Gaussian Performance

A plot of the ensemble averaged, integrated power as a function of bucket radius illustrates the tradeoff between CBC and IBC in more detail. The curves within Fig. 3 show this dependency for the same conditions of Fig. 2 where

<table>
<thead>
<tr>
<th>Category</th>
<th>Parameter</th>
<th>Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Laser</td>
<td>Wavelength</td>
<td>1.07 ( \mu m )</td>
</tr>
<tr>
<td></td>
<td>Aperture configuration</td>
<td>6 Circular subapertures in a 32 cm on-axis beam director</td>
</tr>
<tr>
<td></td>
<td>Total power</td>
<td>160 Hz Error rejection, 320 Hz Error rejection, both with 6 dB overshoot</td>
</tr>
<tr>
<td>Beam control</td>
<td>Track bandwidth (no AO), With AO</td>
<td>160 Hz Error rejection 320 Hz Error rejection 6 dB overshoot</td>
</tr>
<tr>
<td></td>
<td>Adaptive optics, actuator spacing in exit pupil</td>
<td>0.02 m</td>
</tr>
<tr>
<td></td>
<td>Adaptive optics, actuator grid</td>
<td>16 \times 16</td>
</tr>
<tr>
<td></td>
<td>Adaptive optics, bandwidth</td>
<td>200 Hz Error reject, 6 dB overshoot, Type 1*</td>
</tr>
<tr>
<td>Subaperture</td>
<td>Piston jitter, ( \sigma_p )</td>
<td>0.0, 0.13, and 0.4, ( \lambda ) RMS</td>
</tr>
<tr>
<td>Phase error</td>
<td>Tilt jitter, ( \sigma_T )</td>
<td>0.0, 0.1, 0.2, 0.4( \lambda / d ) RMS</td>
</tr>
<tr>
<td></td>
<td>Beam quality, BQ</td>
<td>1.0, 1.22, and 2.20</td>
</tr>
<tr>
<td>Full aperture</td>
<td>Tilt jitter, LOS( \gamma )</td>
<td>0.0, 5.0 ( \mu ) radians RMS</td>
</tr>
<tr>
<td>Atmosphere</td>
<td>Location</td>
<td>Kandahar, Afghanistan</td>
</tr>
<tr>
<td></td>
<td>Season/time of day</td>
<td>Summer/0600, Summer/1500</td>
</tr>
<tr>
<td>Engagement</td>
<td>Air to surface ranges</td>
<td>2.5, 5, 7.5 and 10 km</td>
</tr>
<tr>
<td></td>
<td>Surface to air ranges</td>
<td>2.5, 5, 7.5 and 10 km</td>
</tr>
<tr>
<td></td>
<td>Surface to surface ranges</td>
<td>2.5, 5, 7.5 and 10 km</td>
</tr>
</tbody>
</table>

*Type 1: one free integrator in the forward control loop.*
the array is focused onto a 5 cm diameter bucket at 7.5 km. Since Eq. (3) assumed a uniform field over each subaperture, the plot shows the integrated irradiance for both uniform and an optimally-truncated Gaussian waveform (i.e., 2.25 times the beam waist). Both contain the same power out of the exit pupil. The solid lines are for the coherent case and the dotted curves are for incoherent combining. The first point is that the uniform wave provides more energy on target within the smaller buckets (note, describing this in terms of angular extent takes the range consideration out of the description) than the Gaussian waveform for CBC. It is only when bucket radii become relatively large that a Gaussian waveform surpasses integrated power of a uniform waveform for CBC. This point is moot, though, since IBC surpasses the integrated power of CBC for either Gaussian or uniform waveforms. Clearly, as the bucket size for BPE approaches the central lobe for a single subaperture, the integrated power of an array with Gaussian beams will exceed that of a uniform beam whether one considers the case for CBC or IBC. But, for these bucket sizes, the comparison between CBC and IBC breaks down since the aperture is not a free parameter in the analysis. The consideration of bucket sizes for BPE that approach the central lobe of a single subaperture implies that the wrong aperture geometry has been defined for the system. The conclusion: range and bucket size are key parameters that must be part of the definition of the aperture geometry. Once determined, CBC will provide the better BPE over IBC, regardless of beam shape. The analytical treatment using a uniform field is only a gauge for the best possible BPE since a uniform field (CBC or IBC) provides the higher power densities for the smaller bucket sizes. In the simulations that follow, a Gaussian beam is used due to the practicalities of waveguide lasers.

The consideration to optimize far field irradiance over a given angular extent in the far field opens up a new design dimension for DE systems not available in a monolithic beam design. The analysis within this work assumes that energy coupling into the target is limited to the first few radii of the coherent central lobe of the full aperture.

### 3.3 CBC and IBC versus Bucket Size and Range

The relationship between PIB and BPE is just the normalizing factor of total power out of the aperture, which for this case is 60 kW. What follows is given in terms of PIB to show the marginal differences between CBC and IBC as the angular extent of the bucket is made large. The comparison of PIB...
for a fixed radius bucket as the range increases is presented in Fig. 4. This figure contains PIB(z) for two bucket sizes and for both cases CBC and IBC. The bucket sizes are 5 and 10 cm and the PIB is for the vacuum case. Since the bucket size is fixed, as the range increases the angular radius decreases and eventually only encloses the central lobe of the coherent full aperture. This is manifest in the CBC curve for the 5 cm bucket size at 6 km where the curve levels off. The PIB level at this inflection is dependent on the ‘fill factor,’ $F_f$, of the array. For the uniform subaperture field, the fill factor is defined as the ratio of the total subaperture area divided by the total area that encloses the subapertures. The fill factor for the system in Fig. 1 is calculated in Eq. (4) as,

$$F_f = \frac{n\pi(d/2)^2}{\pi(D/2)^2} = 0.586.$$  

The value of PIB for CBC and for the given fill factor is then

$$\text{PIB}_{\text{CBC}} = 0.586 \times 0.84 \times 60e^3W = 29.5 \text{ kW}.$$  

This agrees with the analytical model calculation in Fig. 4. The 0.84 factor is the percent of power of a monolithic circular aperture within the central lobe of the far field spot.

PIB differences, CBC-IBC, for the two bucket sizes, shown in Fig. 5 more readily displays the performance difference between the two methods of beam combining. CBC is providing more power in the defined bucket than IBC when the curves are positive. For ranges where the angular radius of the bucket is relatively small, the CBC captures more PIB than IBC. In general, these are typical bucket sizes well below the central lobe of a single subaperture. As discussed in Sec. 3.2, for large angular bucket sizes, these curves clearly show that IBC captures more power than CBC. But, again, to conclude that IBC is better than CBC for the close in ranges is to miss the point that a CBC design for this range and bucket size can be defined to outperform IBC. Also, the differences are marginal for the shorter ranges and CBC clearly provides performance out to significantly further distances.

### 3.4 Exit Pupil Scaling

The previous discussion established design considerations for identical geometries given target ranges and vulnerable area diameters. The following establishes a framework to understand the design trade-offs for changes to the exit pupil geometries. The PIB for various configurations of the exit pupil are shown in Fig. 6. All configurations transmit the same amount of power. The solid curve is the encircled power for the IBC case for six subapertures. The dotted curve just above the solid line is the encircled power for the CBC case. These represent the baseline design of Fig. 1 and are the same curves for uniform subaperture illumination as shown in Fig. 3. If the fill factor is changed by reducing the subaperture diameter and then using two rings to fill the 30 cm exit pupil, the first plateau rises indicating the higher power densities due to the increased fill factor. If instead, the same fill factor is maintained, but decreasing the exit pupil diameter by a factor of 3, changes the PIB curve to the dashed line.
scaled down by a factor of 3, the encircled power is now spread out to the wings lowering the power density in the center (shown as the dashed line). (Not shown is the IBC case for the 18 subapertures. This curve would have fallen well below the 6-subaperture IBC case.)

This single plot displays the key tradeoffs for exit pupil geometries when comparing CBC and IBC. The comparison clearly shows that fill factor raises the power density near the center of the optical axis while keeping the same fill factor but reducing the size of the exit pupil diameter scales the power density by the same ratio as the change of diameters, but to larger angles in the far field. Note that the two 6 element arrays plateau at the same level, but the smaller aperture does so at a larger radius.

3.5 Aperture Mismatch

The architecture presented in Fig. 1 uses a full aperture tracker to provide tilt corrections for the subaperture point-sers. This is proposed for design economy and simplicity. However, since the subapertures are smaller than the whole aperture used by the tracker and since they are displaced from the centerline of the tracker line-of-sight (LOS), their pointing will be incorrect to some degree. The magnitude of this error is dependent upon the tracker error rejection bandwidth, turbulence strength, and the effective crosswind. Reference 13 provides a complete development of this error with further study in Refs. 14 and 15. The analysis in this work considers the three scenarios defined in Sec. 2.2.

Recall, they are described as air-to-surface (A2S), surface-to-air (S2A), and surface-to-surface (S2S). The curves presented in Fig. 1 are for the case of no AO and plot RMS tilt error for an individual subaperture as a function of tracker error rejection bandwidth. The errors decrease initially as the tracker error rejection bandwidth increases. For the geometry described in the paper, the errors reach near minimum value at a bandwidth of around 50 Hz. Any further increase in the error rejection bandwidth does not reduce the tilt error appreciably since the correlation of tilt between the mismatched pupils is lower for the higher frequencies. Note with no AO, the magnitude of the minimum error can be quite high for the S2A and S2S scenarios. For these scenarios the error ranges from 0.4$\lambda$/d to $\lambda$/d, where d is the diameter of a subaperture.

In contrast, the A2S scenario, however, shows a much smaller error of 0.13$\lambda$/d with no AO. The difference in pupil mismatch tilt error between the A2S and the S2A is due to the turbulence strength near the aperture being lower for the A2S scenario. As the beam propagates to the target, any phase effects that would cause a tilt have less path length to manifest as an error. When an AO subsystem corrects for turbulence across the full aperture the tilt error due to pupil mismatch is mitigated significantly. With AO, the minimum error in all 3 scenarios is reduced to approximately 0.1$\lambda$/d. Thus, as a cautionary note, it would not be prudent to implement a candidate design as presented in Fig. 1 for S2A or S2S, for either CBC or IBC, without due consideration of the impact of this error in pointing.

4 Wave Optics Simulations

In the previous section, we used theory to compare and analyze CBC and IBC. Now, we include control loops and all atmospheric effects by using wave optics simulation. The wave optics simulation models the atmospheric turbulence and thermal blooming effects; full aperture tracker and adaptive optics; subaperture residual phase and tilt; and subaperture wavefront beam quality. The wave optics simulations were performed with a detailed model assembled in WaveTrain®. Wave optics simulations normally model coherent waveforms, therefore, a method to model the incoherent array was devised for this work. WaveTrain modeled the coherent and incoherent array with the same simulation structure and modeled each case by adding various amounts of random piston to each subaperture field on a frame-by-frame basis. In this way, low-level disturbances were added to model residual errors of a finite-bandwidth phasing loop for the coherent case while higher levels of piston variation were added to model an incoherent array. For the coherent case, the fields are added in the target plane before calculating the total irradiance. For the incoherent case, the piston variances are large to model temporal incoherence and the subaperture irradiances are added in the target plane to model the lack of coherence between the subapertures.

4.1 Wave Optics Setup

The subaperture waveforms in the simulation are modeled as truncated Gaussian beams since this is expected to well model the likely beam shape from a waveguide source. Each Gaussian beam (also referred to as a “beamlet”) is truncated at $d = 2.25 w_0$, where $w_0$ is the $1/e^2$ irradiance radius of the Gaussian beamlet and $d$ is the diameter of the truncating aperture. The transmitted power at the exit pupil is set after truncation to be the same in all cases. Such truncation produces maximum on-axis intensity for a single laser source. For the case of coherent combination, the optimal sizing would be about $d = 2.13 w_0$. To allow direct comparison of performance, the analysis uses the same size, 2.25$w_0$, for all analysis of CBC and IBC. It should be noted that performance on-axis for CBC could be slightly increased by optimally sizing the beamlets for the CBC case. Performance could also be slightly increased for the cases with tilt jitter, $\sigma_T$, if the beamlets were resized according to Yura’s equations (see Ref. 24). Additionally, the truncation to

![Fig. 7 Subaperture pointing tilt error due to full aperture tracker without AO. The tilt error is a function of both the turbulence and the tracker’s error rejection bandwidth. This tilt error is mitigated significantly when an AO subsystem corrects for turbulence across the full aperture. For all systems analyzed in this work, the error with AO is reduced to less than 1/10 $\lambda$/d, where $d$ is the diameter of the subaperture.](image)
maximize PIB for a certain target size could differ from that to maximize on-axis intensity. The analysis for optimizing PIB as a function of subaperture field is left as a follow on report. In this work, however, the authors do not expect these possible changes in truncation and subaperture fields would alter the conclusions of this paper in any way.

The wave optics simulation includes all effects from exit aperture to the target. A point source is used as a target to simplify the analysis of coherent versus incoherent beam combining. The simulation adds random disturbances to model residual errors that would arise from the system’s local tilt loop for the full aperture, and the tilt and phasing loops of the multilaser source. These disturbances are all considered pairwise independent. Each is modeled as a random variable with an underlying white, Gaussian distribution, with the RMS chosen to vary the magnitude of the disturbance. In addition to these residuals, the beam quality of each subaperture field can be degraded to model less than perfect sources. These disturbances and the effects they model are summarized as follows:

1. LOS Jitter ($\text{LOS}_T$): Full aperture LOS jitter that models unsensed, on-board optical LOS variations due to base disturbances. The magnitude is set by the RMS value, $\text{LOS}_T$, of a white, Gaussian distribution.

2. Subaperture random piston ($\sigma_p$): Array coherence is varied by adding a time varying piston to each subaperture. The magnitude is set by the RMS value, $\sigma_p$, of a white, Gaussian distribution. The RMS is varied in magnitude to simulate a coherent array with a low residual phase loop error or with large values to simulate an incoherent array.

3. Subaperture random tilt ($\sigma_T$): This effect models residual tilt jitter from the on-board beam relay loop (not shown in Fig. 8). The magnitude is set by the RMS value, $\sigma_T$, of a white, Gaussian distribution.

4. Subaperture beam quality (BQ): WaveTrain® models higher-order phase aberrations each subaperture to account for reduced beam quality in each of the array sources. The beam quality phase is generated by summing Zernike polynomials of order 4 to 15 (Noll’s ordering) with each radial order receiving an equal weighting of net wavefront variance totaling to $\sigma_{\text{WFE}}^2$. Beam quality uses the Maréchel approximation and the performance model relating BQ to Strehl to arrive at the relationship $\text{BQ} = \exp\left(\sqrt{2\pi\sigma_{\text{WFE}}^2}\right)$.

The system degradations described above are used to model realistic systems and to evaluate the sensitivity of the system to these residuals. The wave optics simulation with the defined residuals then provides an evaluation of BPE. This metric is evaluated for three different scenarios, each for two different atmospheric conditions. The performance of a fully-coherent, idealized laser array would be simulated with the residual disturbance parameter set with $\text{LOS}_T = 0$, $\sigma_p = 0$, $\sigma_T = 0$, and $\text{BQ} = 1$.

Figure 8 is an instance of the subapertures’ fields, each with either random piston [Fig. 8(a)], random tilt [Fig. 8(b)], or random higher-order phase error to model a reduction in beam quality [Fig. 8(c)].

The wave optics model also includes control loops for full-aperture tracking and adaptive optics. The full transmitting aperture is used to collect target radiance and is spatially shared with a single, full aperture tracker and adaptive optics (AO) system. The tracker controls a single fast steering mirror (FSM), which corrects all beamlets using the measured, full aperture tilt of the line-of-sight (LOS) to the target. The tracker has two bandwidths: 160 Hz error rejection for track only mode and 320 Hz when the AO subsystem is closed loop. Both loops have a nominal 6 db of overshoot. The higher tracker bandwidth was used to accommodate the higher frame rates used for the AO subsystem.

The AO subsystem uses full aperture measurements with a Shack-Hartmann wavefront sensor (WFS) and a single deformable mirror (DM) to correct for higher order atmospheric disturbances. The DM has a 16×16 square grid of actuators truncated by the 32 cm diameter aperture. The AO error rejection bandwidth is 200 Hz with 6 db of overshoot. The analysis to follow will report results with and without the AO in operation. A list of pertinent parameters for the laser aperture and beam control subsystem are given in Table 1. Figure 9 shows, qualitatively, the effect of AO can have on both CBC and IBC far-field spots for the surface to air case at 7.5 km range with no subaperture phase errors or platform jitter. The right column is IBC, while the left is CBC. The first row shows the far-field spots with no turbulence, while the second row includes turbulence, visibly degrading both CBC and IBC spots. The last row includes both turbulence and AO, showing that AO does reduce turbulence degradations.

---

**Fig. 8** The OPD of the beamlets for incoherence, tilt jitter error, and imperfect beam quality: (a) shows the OPD for incoherent combination ($\sigma_p = 0.4\lambda$) for a single time instance, (b) shows the OPD with $0.4\lambda/d$ differential jitter ($\sigma_T$), and (c) shows the OPD for poor beam quality (BQ = 2.20).
4.2 Description of Atmospheric Conditions

The atmospheres chosen for this work are based on parameter and particle distributions constructed by the laser environmental effects definitions and reference (LEEDR) software package using the ExPERT database. The ExPERT database contains world-wide, climatological data recorded over approximately the last thirty years for 573 worldwide sites. LEEDR uses the observations recorded at these sites to estimate the average transmission within the boundary layer for each location. After forming a cumulative distribution of transmissions at the 1.07 μm wavelength, we selected a value close to the worldwide median for tactical engagements. The surface conditions associated with this site provided a consistent parameter set to model the most probable atmospheric condition. The site associated with the median transmission was Kandahar, Afghanistan.

LEEDR provided high-fidelity profiles of absorption, scattering, and turbulence for the selected atmospheres at 1.07 μm. Figure 10 shows the two components of atmospheric extinction, absorption and scattering, for the two selected profiles above Kandahar, one for 0600 and the other for 1500 local time. As the surface temperature rises, the atmospheric conditions change, affecting the transmission and propagation of laser beams. The figures illustrate the importance of accurate atmospheric modeling in laser engagement scenarios.
in the afternoon, the boundary layer height and thickness increases accompanied by a corresponding increase in turbulence. LEEDR modifies the lower portion of the Hufnagel-Valley (HV) profile to account for the change in turbulence strength as the surface temperature increases. This modification is based on the McClung-Tunick model developed by the Air Force Institute of Technology, which more accurately accounts for turbulence in the first 50 m above the surface. Above 50 m, the turbulence profile blends with the Hufnagel-Valley 5/7 profile. Figure 11 shows the turbulence profiles used for the two different times. Note that below 50 m altitude at 0600, the predicted turbulence levels are lower than the HV 5/7 profile. The results presented in Sec. 5 use the atmospheric conditions for Kandahar for 0600 and 1500 local to represent a moderate and a high turbulence case, respectively.

4.3 Numerical Considerations

The wave optics simulation is the most appropriate method for analysis beyond what can be done with theory, but requires due consideration in generating reliable results. Recognizing that $C_n^2$ is only a parameterization of the variability of a given atmosphere, a performance data point for PIB consists of an average over thirty experiments of the same scenario with each experiment using a different random realization of the atmosphere for the given $C_n^2$. The PIB calculated from a single experiment is the average PIB over the last 50 ms of the time simulation. Choosing the last 50 ms of PIB in the experiment avoids transients due to the tracker and AO responses and ensures the thermal model of the beam-atmosphere interaction has reached steady-state. Figure 12 displays the variability in PIB (dots) over different atmospheric realizations (i.e., for 30 different experiments) for the surface to air engagement. The solid line is the running average of the PIB over the experiment number. The dotted curves enclosing the running mean of PIB show the 95% confidence interval. Table 3 shows the percentages for 95% confidence intervals for the three scenarios. The limits shown bracket the confidence intervals calculated for the three scenarios for the moderate and high turbulence atmospheres. The conditions for the two intervals are listed in the table. The greatest variability occurs for the S2S scenario with a confidence interval just under 10%. Most others remain around 5%. The results reported for all cases in the remaining sections can be considered to have a 95% confidence interval for BPE when $+/−10%$ of the values reported is applied.

5 Simulation Results and Comparison with Theory

In this section, we use the wave optics simulations just described to analyze performance of the conceptual system.
architecture of Fig. 1 for both CBC and IBC. The assumption adhered to is that the aperture diameter is given and fixed. This is not unreasonable, since the size of the beam director will be a major driver in system performance, its size would be made as large as feasible to extend range and reduce the effects of diffraction. The theory-based curves shown in Figs. 2 and 3 clearly show that for the vacuum case and for the given fixed aperture geometry, CBC will always perform better than IBC for bucket sizes less than a few times the radius of the vacuum far field central lobe of the synthesized aperture.

Table 4 contains a partial summary of results comparing CBC and IBC starting with the vacuum case and successively including additional atmospheric effects. Tables and show the associated atmospheric and performance parameters commonly used to predict tracking and AO performance. The atmospheric and system parameters for each simulation are listed within Table. The sequential decrease in performance with the inclusion of more effects provides a look at the sensitivity of the system and an upper bound for corrective measures. This summary shows that under both moderate and high turbulence, CBC outperforms IBC. In some cases the performance increase may not justify the additional complexity of the phasing subsystem or the AO subsystem. It can also be noted from Table 4 that the CBC S2A case shows a significant loss due to atmospheric turbulence. This tags this scenario for consideration of an AO subsystem. Recall that with the absence of AO there is a reduction in BPE performance due the mismatch of pupils. The addition of AO will not only improve performance by correcting the higher order, but also in this case, by improving the subaperture pointing. Further, Table 4 shows that the S2S scenario is dominated by turbulence, as the addition of turbulence has by far the most degrading impact on BPE. Note the only slight reduction in the A2S scenario in turbulence implies AO may not be considered for a system that only flew A2S scenarios. Table 4 shows that for the 60 kW power level, thermal blooming has little impact on performance for all scenarios. An increase in power level is explored further in a later section. Lastly, note that the omission of BPE for the high turbulence S2S scenario. This is a stressing case for both CBC and IBC, but IBC, in general, will be more limited in range even with AO. This scenario is referred to as ‘deep turbulence’ and is the subject of ongoing research for CBC. Figure 13 presents BPE for both CBC and IBC for all three scenarios as a function of range. These plots clearly show the benefit of CBC over IBC. The log scale for performance reduces the graphical differences between CBC and IBC, also, we remark that BPE performance below 10% is not considered a viable mission.

### Impact of Subaperture Piston and Tilt Error, \( \sigma_p \) and \( \sigma_T \)

The performance of CBC has been so far reported without residual errors that would be present in the phasing and pointing loops due to finite bandwidths. The next few

**Table 3** Ninety-five percent confidence interval bounds (%) for the 7.5 km slant range.

<table>
<thead>
<tr>
<th>Engagement</th>
<th>Air to surface</th>
<th>Surface to air</th>
<th>Surface to surface</th>
</tr>
</thead>
<tbody>
<tr>
<td>Turbulence</td>
<td>Moderate</td>
<td>High</td>
<td>Moderate</td>
</tr>
<tr>
<td>Bucket diameter</td>
<td>5 cm, 10 cm</td>
<td>5 cm, 10 cm</td>
<td>5 cm, 10 cm</td>
</tr>
<tr>
<td>Benign case</td>
<td>2.75, 0.98</td>
<td>2.92, 1.36</td>
<td>2.36, 0.80</td>
</tr>
<tr>
<td>Stressing case</td>
<td>5.80, 2.78</td>
<td>5.89, 3.23</td>
<td>5.51, 2.15</td>
</tr>
</tbody>
</table>

\( a \)The benign case has zero piston error, zero subaperture tilt, a BQ of 1.0, no platform LOS jitter, and AO on. This combination generally produces the smallest confidence interval bounds.

\( b \)The stressing case is for incoherent combining and has 0.4 waves RMS piston error, 0.4 lambda/d differential tilt, a BQ of 2.2, 5 urad rms full aperture LOS jitter, and AO off. This combination generally produces the largest confidence interval bounds.

**Table 4** BPE (%) for 60 kW, 7.5 km slant range, moderate and high turbulence, LOS = 0, \( \sigma_p = 0, \sigma_T = 0 \), and BQ = 1, full aperture tracker, no AO.

<table>
<thead>
<tr>
<th>Engagement</th>
<th>Air to surface</th>
<th>Surface to air</th>
<th>Surface to surface</th>
</tr>
</thead>
<tbody>
<tr>
<td>Coherence</td>
<td>Incoherent</td>
<td>Coherent</td>
<td>Incoherent</td>
</tr>
<tr>
<td>Bucket diameter</td>
<td>5 cm, 10 cm</td>
<td>5 cm, 10 cm</td>
<td>5 cm, 10 cm</td>
</tr>
<tr>
<td>Diffraction-limited</td>
<td>17.5, 55.1</td>
<td>44.4, 64.0</td>
<td>17.5, 55.1</td>
</tr>
<tr>
<td>Diff. and extinction</td>
<td>10.9, 34.3</td>
<td>27.6, 39.8</td>
<td>10.9, 34.3</td>
</tr>
<tr>
<td>Diff., ext., and moderate turbulence</td>
<td>10.3, 32.5</td>
<td>24.4, 37.9</td>
<td>6.3, 21.2</td>
</tr>
<tr>
<td>All above effects with thermal blooming</td>
<td>8.9, 29.0</td>
<td>22.2, 34.6</td>
<td>5.6, 19.5</td>
</tr>
<tr>
<td>All effects, high turbulence</td>
<td>8.3, 27.5</td>
<td>19.9, 32.4</td>
<td>1.5, 5.5</td>
</tr>
</tbody>
</table>
sections present a sensitivity study to the magnitude of these residuals, starting with the subaperture phase and tilt errors. The theoretical curves are plotted with use of Eq. (3) adjusted for atmospheric extinction over the 7.5 km path.

Figure 14 separately shows the sensitivity to subaperture tilt jitter, $\sigma_T$, and piston jitter, $\sigma_p$. As a point of reference, consider the A2S scenario. BPE is reduced by $\sim 10\%$ when all subapertures have a residual tilt jitter of $0.2\lambda/d$ RMS. This is considered significant and would require care in design, but not necessarily a stressing design requirement. Note the increased sensitivity to piston jitter versus subaperture tilt jitter, but even with large increases in piston jitter, the BPE asymptotes to a level defined by the IBC of the array. This level can be seen in the figure to be a BPE of about 15% occurring at an RMS value of $0.28\lambda$. For the A2S CBC scenario, keeping the reduction in BPE less than $\sim 10\%$ due to piston jitter alone requires an RMS value below $0.1\lambda$. Given published results for phasing multiple sources report $0.03\lambda$ RMS or better in a laboratory environment this requirement is not considered stressing.

Since the BPE plot versus piston RMS jitter in Fig. 14(b) spans values equivalent to an incoherent array, a comparison of IBC to CBC can be made by comparing the values to the right of $0.28\lambda$ RMS to those left of this point for CBC.

5.2 Impact of Beam Quality, BQ

The analysis included beam quality residual errors to specifically determine if its effects would be masked by moderate or high turbulence. The analysis that follows shows that beam quality directly impacts BPE even in strong turbulence and a reduction in beam quality is not masked with other beam spreading effects in a root-summed-squared (RSS) relationship. Figure 15 shows the dramatic drop in performance for both CBC [Fig. 15(a)] and IBC [Fig. 15(b)] for all three engagements as beam quality degrades for the case of a 7.5 km slant range, a 5 cm diameter bucket, and moderate turbulence.

Figure 15(a) shows BPE drops by 70% for the CBC air to surface case ($30.0$ cm $r_0$) as beam quality is reduced from 1.0 to 2.2. For the surface to surface engagement ($4.28$ cm $r_0$), the same change in beam quality reduces BPE by 54%. Figure 15(b) shows similar trends for IBC. Again, poor beam quality for IBC results in reduced performance for all engagements. Since BPE for IBC is lower than CBC for the better beam quality values, the reduction is less dramatic but still measurable.

5.3 Impact of Platform Jitter, LOS$_T$

Residual error in platform jitter is one of the major contributors to loss of energy on target in all laser systems. The effects of subaperture jitter, $\sigma_T$, have already been presented, this section presents the impact when all beamlets are moving in unison, i.e., as coherent tilt jitter, previously presented.

### Table 5

<table>
<thead>
<tr>
<th>Time of day</th>
<th>Engagement</th>
<th>Rytov value</th>
<th>Fried $r_0$ (m)</th>
<th>Greenwood (Hz)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0600</td>
<td>Air to surface</td>
<td>0.0733</td>
<td>0.300</td>
<td>34.3</td>
</tr>
<tr>
<td></td>
<td>Surface to air</td>
<td>0.0733</td>
<td>0.0692</td>
<td>36.7</td>
</tr>
<tr>
<td></td>
<td>Surface to surface</td>
<td>0.596</td>
<td>0.0428</td>
<td>62.2</td>
</tr>
<tr>
<td>1500</td>
<td>Air to surface</td>
<td>0.225</td>
<td>0.252</td>
<td>57.5</td>
</tr>
<tr>
<td></td>
<td>Surface to air</td>
<td>0.2252</td>
<td>0.0264</td>
<td>61.6</td>
</tr>
<tr>
<td></td>
<td>Surface to surface</td>
<td>18.17</td>
<td>0.0055</td>
<td>482</td>
</tr>
</tbody>
</table>

### Table 6

<table>
<thead>
<tr>
<th>Time of day</th>
<th>Range (m)</th>
<th>$r_0$ (m) Air to surface</th>
<th>$r_0$ (m) Surface to air</th>
<th>$r_0$ (m) Surface to surface</th>
</tr>
</thead>
<tbody>
<tr>
<td>0600</td>
<td>2500</td>
<td>0.554</td>
<td>0.133</td>
<td>0.0827</td>
</tr>
<tr>
<td>0600</td>
<td>5000</td>
<td>0.366</td>
<td>0.0876</td>
<td>0.0546</td>
</tr>
<tr>
<td>0600</td>
<td>7500</td>
<td>0.300</td>
<td>0.0692</td>
<td>0.0428</td>
</tr>
<tr>
<td>0600</td>
<td>10000</td>
<td>0.241</td>
<td>0.0578</td>
<td>0.0361</td>
</tr>
</tbody>
</table>
defined as full aperture tilt jitter, LOS\(_T\). Since a poorer BQ will cause a spreading of the far field beam, BQ is varied in conjunction with full aperture tilt to investigate the performance combination of these two effects.

Figure 16(a) shows the BPE with LOS\(_T\) \(= 5\) urad (RMS) for all three engagements and BQ \(= 1.0, 1.22,\) and 2.20. These results are compared to zero LOS\(_T\) in Fig. 15 reprinted to the left of Fig. 16(a) for easy reference. It can be seen that LOS\(_T\) significantly reduces BPE from 22% to 12% for the A2S scenario with BQ \(= 1\). S2A and S2S result show similar drops in performance due to LOS\(_T\) and all scenarios show similar percentage drops in BPE with BQ reductions as seen without a full aperture tilt (Fig. 15). It should be noted that the jitter being \(1.6\lambda / D\) is high and demonstrates that BQ cannot be relaxed without reducing performance even in the presence of large tilt RMS’s.

The same comparison is made in Fig. 17 for the IBC case. For the IBC case the impact of LOS\(_T\) jitter is reduced since the diffraction angle is much larger, approximately three times that of the CBC. Both simulations were run under the same conditions of moderate turbulence.

Figure 18 completes the sensitivity for IBC. The turbulence is high, the full aperture pointing error is high with LOS\(_T\) \(= 1.66\lambda / D\), the subaperture pointing error is moderate with, \(\sigma_T = 0.24\lambda / d\), and \(\sigma_p\) is near zero at 0.01\(\lambda\). The high turbulence dominates the reduction in performance, but all effects contribute to a reduction in performance which is considered not viable (BPE <10%) for all scenarios except A2S. However, even under these conditions, a reduction in beam quality is still measurable for A2S and S2A. Note these results do not use AO, and BPE is now measured over a 10 cm bucket. The fact that AO is not employed and the larger, 10 cm bucket is used, favors a reduction in sensitivity to BQ changes, yet the results still show an impact on performance for these two scenarios. For the A2S engagement, reducing BQ from 1.0 to 2.2 reduces BPE by 52%. These results are presented for completeness, but it is questionable that a system with such a low BPE would be considered useful once it falls well below 10%. Therefore, for any tactical laser system, beam quality will be a major driver of overall system performance.

5.4 Impact of Adaptive Optics

Simulation results show the addition of an AO system significantly improves the performance of both CBC and IBC. The design used in the analysis has an actuator spacing of 2.0 cm in exit pupil space. Using a Fried geometry, this has approximately 5 actuators across each 10.0 cm diameter beamlet. Figure 19 presents AO performance for coherent combination for the moderate turbulence case as subaperture tilt [Fig. 19(a)] and piston jitter [Fig. 19(b)] are added.
A2S scenario has the highest BPE before AO is applied and, as expected, its performance changes the least with the addition of AO. The addition of AO in the A2S scenario has little impact on performance improvement since the turbulence strength, in this case, being stronger closer to the target has little impact on irradiance in the target plane. Note, however, for the other scenarios that AO consistently improves the performance of CBC for both tilt and piston jitter. In these cases the performance increase is due to the correction of the higher order atmospheric effects and pupil mismatch.

With AO employed, the phasing loops are the only difference between CBC and IBC and, thus, the sensitivity plot of Fig. 19 (b) can be used to compare CBC and IBC with AO. Referencing this figure, it can be seen that piston jitter at 0.4\(\lambda\) can be directly compared to CBC-performance points to the left of 0.28\(\lambda\). Since the AO subsystem does not correct for residual subaperture piston jitter (thus, the downward trend in Fig. 19 (b)), this is the only difference between IBC and CBC. With this mind, the lower IBC performance can be understood in terms of adaptive optics where the individual beamlets are subapertures of a full aperture AO system, but in this case, subaperture tilt is only corrected. Hardy
remarks that piston errors between subapertures in an AO subsystem are more detrimental than subaperture tilts in AO corrections. The higher order phase across the full aperture of CBC and IBC, including tilt errors due to pupil mismatch, are corrected up to the random piston over each beamlet. Considering the individual beamlets of the IBC as a sparse AO subsystem the observation from Hardy provides another way to understand the performance difference between CBC and IBC when AO is used. Figure 20 summarizes the performance increase with the inclusion of AO. As explained, AO improves both S2A and S2S significantly in moderate turbulence with little impact on A2S.

5.5 Impact of Thermal Blooming

Thermal blooming is the nonlinear interaction of the beam intensity with the atmosphere. The localized heating of the air, as the beam transits to the target, changes the index of refraction and causes a distortion of the beam along its path. The salient features of tilt and astigmatism in the far field spot can only be partially corrected for with an AO subsystem. The increased density of the lower atmosphere makes this effect more severe as the path becomes more horizontal. In this section the sensitivity to thermal blooming is investigated. All results presented previously included this effect inherent to the atmosphere. The values shown for S2S scenario for a range of 7.5 km and with high turbulence is out of reach with conventional AO. S2A shows significant improvement since the turbulence, weighted closer to the exit pupil of the transmitter, can be corrected more easily than the other scenarios. Conversely, the turbulence being weighted further from the transmitting aperture for the A2S shows little change in performance.
to follow the comparison is made with thermal blooming turned off and on within the simulation.

The magnitude of thermal blooming has traditionally been qualitatively defined with the distortion number, \( N_d \). Definitions of \( N_d \) vary in the literature depending on the author’s preference as to which effects are most important to model. The definition chosen for this work is described in Ref. 3. The integral for \( N_d \) is defined in Eq. (4). This equation is based on a monolithic beam, thus, it is presented here with the cautionary note that its fidelity in representing a multilaser beam has not yet been evaluated. In addition to \( N_d \), another parameter that gauges the effect of thermal blooming is critical power. This is the level of power above which the effect of thermal blooming dominates transmission and any further increase in power could cause even less power to arrive on target.

\[
N_d = 4\sqrt{2} P_k \frac{(n_0 - 1)}{C_p \rho_0} \int_0^{\text{path}} dz \frac{\alpha_{\text{abs}}(z) \tau(z)}{T(z) D(z) v(z)}, \tag{5}
\]

where \( P \) is power out of the aperture, \( k \) is \( 2\pi/\lambda \), \( n_0 \) is the refractive index of the undisturbed atmosphere, \( C_p \) is the specific heat at constant pressure, \( \rho_0 \) is the air density at mean sea level, \( \alpha_{\text{abs}} \) is the absorption coefficient, \( T(z) \) is the temperature of the air, \( D(z) \) is the diameter of the beam along the path, \( v(z) \) is the effective crosswind along the path, and \( \tau(z) \) is the transmission along the path.

The distortion numbers and critical powers for the three scenarios and the two power levels used in this work are shown in Table 7. Figure 22(a) and 22(b) shows the performance decrease in BPE for CBC and IBC for a 60 and 150 kW array, respectively. The 60 kW power level shows minimal impact on BPE for all scenarios due to thermal blooming. The largest magnitude in reduction due to thermal blooming occurs for the A2S scenario at the 150 kW level with a reduction in BPE from 24% to 16%. This dramatic decrease in performance is most likely due to the following. The reduction of the turbulence strength with an increase in altitude favors the A2S scenario. But, unlike the turbulence, the absorption within the boundary layer is fairly constant in altitude, thus, the A2S beam, less spread than in the other two scenarios, will bloom more due to the beam’s higher power density. The S2A and the S2S have been degraded already by the turbulence and, thus, show much lower reduction due to thermal blooming.

The distortion numbers and critical powers calculated for these scenarios are not consistent with the simulation results. A full explanation is still being explored, but two comments are appropriate. First, the starting performance for all IBC scenarios are low (10% or lower) and adding the additional effect of thermal blooming has low impact. Second, it appears that use of the Eq. (4) over estimates the reduction in performance for a laser array.

5.6 Analysis of System Performance

This section selects nominal values for the set of parameters used in the previous sensitivity studies and reports the performance for the three scenarios as a function of range, both with and without AO included. This last look at performance is restricted to the CBC since it has been shown to be an upper bound for IBC for all previously presented results.

Figure 23 presents performance for the three scenarios as a function of range with all disturbances included and set to reasonable values listed in Table 8. A far field pattern provided to the right of Fig. 23 shows a BPE of \(~10\%\). This is an average of far field performance for the A2S scenario at a range of 7.5 km. Given a 10% BPE as a minimally accepted performance, the maximum ranges for the three scenarios are presented in Table 8.

6 Summary

This paper provides a framework to study the performance tradeoffs for CBC and IBC. The design is not optimized for

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Table 7 \( N_d \) and critical power (kW) levels for the three scenarios at 7.5 km slant range.

<table>
<thead>
<tr>
<th>Engagement</th>
<th>Air to surface</th>
<th>Surface to air</th>
<th>Surface to surface</th>
</tr>
</thead>
<tbody>
<tr>
<td>Power level (kW)</td>
<td>60</td>
<td>150</td>
<td>60</td>
</tr>
<tr>
<td>( N_d )</td>
<td>14</td>
<td>37</td>
<td>16</td>
</tr>
<tr>
<td>Critical power (kW)</td>
<td>111</td>
<td>105</td>
<td>97</td>
</tr>
</tbody>
</table>

Fig. 22 BPE with and without the effects of thermal blooming on CBC and IBC. (a) The 60 kW system and (b) the 150 kW system. For the A2S CBC case, thermal blooming reduced BPE from 24 to 22 for the 60 kW array and from 24 to 16 for 150 kW array (all numbers percentages). Simulation conditions: are 7.5 km range, 5 cm bucket, moderate turbulence, LOS\(_r\) = 0, \( \sigma_r \) = 0, \( \sigma_p \) = 0 or 0.4\( \lambda \), BQ = 1.0, and no AO.
coherent beam combining, but rather was based on previous architectures in the literature. More importantly, this pupil geometry allows for a clear presentation of the tradeoffs between coherent and incoherent beam combining.

The adaption of previous work by Butts18 provides an analytical description that captures both configurations, CBC and IBC, in a single equation. The tuning of a single parameter, $\sigma_p$, that models random phase between the individual beamlets, allows for a direct comparison in a vacuum of the two systems without approximation. Additionally, the analytical model provides a first-cut at setting design requirements for acceptable levels of subaperture RMS piston and tilt errors.

The same equation can be numerically integrated to calculate the performance metric of beam propagation efficiency, BPE. This metric captures the performance effect that best describes the transmitter performance in depositing energy within a defined bucket size in the far field. The analytical form is restricted to the vacuum case, but numerically integrated, it is used as an envelope of performance for follow-on wave optics simulation.

For identical pupil configurations, CBC typically performs better than IBC. The analysis shows this is true for bucket radii that are a few times the diffraction-limited width of the full aperture far-field spot. The effects of varying fill factor and aperture size when comparing CBC and IBC is explained within the report. A graphical presentation (Fig. 6) clearly demonstrates the tradeoff.

Three scenarios were evaluated to cover the complete set of generic tactical operations. Realistic power levels of the waveguide lasers for the beamlets were chosen for a 60 kW system and soon-to-be-demonstrated levels were considered for a 150 kW system. A median atmosphere for transmission was chosen from a worldwide database to maintain a consistent set of atmospheric parameters. A modified Hufnagel-Valley turbulence profile better accounting for the heating of the earth’s boundary layer provided two atmospheres with moderate and high turbulence for a morning and afternoon scenario time, respectively.

The moderate turbulence atmosphere was used for the majority of the analysis. Performance was degraded significantly under the high turbulence atmosphere (Fig. 6), and the very low BPE numbers that resulted suggest that conventional AO is inadequate for this condition, except for S2A. The S2S scenario, not surprisingly the most stressing of the three, was dominated by turbulence degradation, even for moderate turbulence.

The impact of poor BQ was evaluated under moderate to severe conditions, including system random errors and high turbulence conditions. Beam quality significantly affected performance under all reasonable turbulence levels. In comparison, the impact from typical levels of platform jitter was found to be less significant (Fig. 7). In all cases evaluated, a poorer BQ decreased performance. This conclusion implies that BQ, as a system performance parameter, may not

### Table 8 Nominal system parameters.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Setting</th>
</tr>
</thead>
<tbody>
<tr>
<td>Power</td>
<td>60 kW</td>
</tr>
<tr>
<td>Turbulence</td>
<td>Moderate</td>
</tr>
<tr>
<td>$\text{LOS}_{T}$</td>
<td>$0.3/\lambda D$</td>
</tr>
<tr>
<td>$\sigma_T$</td>
<td>$0.1/\lambda d$</td>
</tr>
<tr>
<td>$\sigma_p$</td>
<td>$0.1/\lambda$</td>
</tr>
<tr>
<td>BQ</td>
<td>1.22</td>
</tr>
<tr>
<td>AO</td>
<td>200 Hz</td>
</tr>
<tr>
<td>Tracker</td>
<td>320 Hz</td>
</tr>
</tbody>
</table>

### Table 9 Maximum range for CBC with a BPE of at least 10%.

<table>
<thead>
<tr>
<th>Scenario</th>
<th>Max range (&gt;10% BPE, no AO)</th>
<th>Max range (&gt;10% BPE, with AO)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Air to surface</td>
<td>~8 km</td>
<td>~8 km</td>
</tr>
<tr>
<td>Surface to air</td>
<td>~6 km</td>
<td>~8 km</td>
</tr>
<tr>
<td>Surface to surface</td>
<td>~4.5 km</td>
<td>~6 km</td>
</tr>
</tbody>
</table>
combine with other debilitating effects in a typical root-sum-square relationship.

Subaperture jitter, $\sigma_T$, was of minor significance if limited to 2 $\mu$m RMS or less (Fig. 4). In the S2A scenario, this required the addition of an AO loop to reduce tilt errors due to pupil mismatch. For the A2S scenario, the inclusion of AO had little impact on performance because the turbulence was weighted closer to the target (Fig. 5).

For the sake of brevity and clarity, the analysis in this report did not vary fill factor. The main point concerning fill factor is embodied in Fig. 6 where the effects of its fill factor is embodied in Fig. 6 where the effects of its

References

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