Measurement and comparison of one- and two-dimensional modulation transfer function of optical imaging systems based on the random target method

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Abstract. One-dimensional modulation transfer function (1-D MTF) has been generally calculated to evaluate the image quality of optical imaging systems, such as the horizontal MTF and vertical MTF. These MTFs can be measured by the use of some mature ways. However, the information of 1-D MTF for performance evaluation may not enough for the systems handling two-dimensional (2-D) targets of high resolution, thus discussing 2-D MTF will be necessary. We investigate the measurement method for the 1-D and 2-D MTF of optical imaging systems based on the random target method, and the characteristics of 2-D MTF and 1-D MTF in terms of MTF values and cutoff frequency are also noted.

1 Introduction

Modulation transfer function (MTF) has been widely used to evaluate the image quality of imaging systems because it works in a direct way to reveal the performance of imaging systems. MTF describes the spatial frequency transfer characteristics of imaging systems from object space to image space by employing the contrast value of a series of sine waves with varying spatial frequencies.

There are a lot of mature ways to measure the MTF of optical imaging systems. According to their different templates, MTF test methods can be categorized into different types, such as the knife edge method, the slit method, the bar target method, etc. Generally, these methods’ templates have a common feature in that their image brightness changes in one direction and remains constant in the orthogonal direction, e.g., the U.S. Air Force resolution target. Naturally, the MTF measured with these templates will contain the modulation information in only one direction, such as the horizontal MTF and vertical MTF. In this paper, these MTFs are called one-dimensional (1-D) MTFs and their corresponding templates are called 1-D templates.

In 2010, Marom et al. proposed a new kind of two-dimensional (2-D) template which looks like a checkerboard measuring the “true characterization” of some systems, for example, the barcode scanning system. Marom et al. explained that a 2-D template is different from a 1-D template because its image brightness changes in two orthogonal directions, and the result of a 1-D contrast transfer function (CTF) for a 2-D template will be affected by the brightness changes in another direction, which will not occur with the 1-D template. Haim et al. proved theoretically and experimentally that the CTF measured by the 2-D template is lower than that obtained with 1-D templates at every spatial frequency and at its cutoff frequency while the former template is $\sqrt{2}$ times the latter one. To maintain consistency, in this paper we adopt Marom’s 2-D template definition in which the brightness of 2-D templates changes in two orthogonal directions.

Recently, the random target method, a new MTF test method, has been applied for image quality evaluation. The method was first proposed by Daniels et al. in which a random image is used as the template, and then it is imaged on a charge coupled device (CCD) by the optical system under test (OSUT). By using the power spectral density (PSD) values of the image captured by a CCD and those of the original image, one can obtain the optical system’s MTF with Fourier spectral analysis. The test method is convenient and fast because the random image has the characteristic of shift invariance and one can easily achieve automatic measurement. The previous works focus mostly on the 1-D MTF test. However, the random image can also be used as a 2-D target since its image brightness changes in two orthogonal directions and is available for measuring 2-D MTF. In 2013, Evtikhiev et al. proposed a new random target to reduce the noise impact for the 2-D MTF measurement.

In this paper, we investigate the measurement for 2-D MTF with the random target method as well as 1-D MTF. A new approach is applied to reduce noise by the use of a significantly large number of random images. The results of the measurement for 1-D and 2-D MTF show that 2-D MTF can be more comprehensive than 1-D MTF when describing the true modulation features of optical imaging systems.

Section analyzes the 1-D and 2-D MTF theoretically and elaborates on the mathematical principles for 1-D and 2-D MTF measurement by using the random target method.
Section 3 presents the procedures of the experiment and the results. Section 4 contains the conclusions.

2 Methodology

2.1 MTF Review and Comparison of 1-D and 2-D MTF

In incoherent illumination systems, the optical transfer function (OTF) is the normalized autocorrelation of the system exit pupil, which can be expressed as

$$\text{OTF}(\xi, \eta) = \frac{\int_{-\infty}^{\infty} P(x, y) P^*(x + \lambda \xi, y + \lambda \eta) dx \, dy}{\int_{-\infty}^{\infty} P(x, y) dx \, dy},$$

(1)

where $P(x, y)$ is the system’s exit pupil function, $\lambda$ is wavelength, and $z_e$ is the distance from the exit pupil plane to the image plane. MTF is the absolute value of the system’s OTF, i.e., $\text{MTF} = |\text{OTF}|$. This is the rigorous definition of MTF. Although one rarely measures MTF through OTF because the OTF test itself is complicated, there is no denying that it is plausible.

MTF describes the spatial frequency transfer characteristics of imaging systems defined as the ratio of the output to the input sinusoidal targets’ contrast value. In this way, one can easily obtain the MTF through detecting the contrast value of input and output sinusoidal targets, but this method is rarely used because it is hard to exactly and efficiently fabricate sinusoidal targets. In our work, to reveal the internal relationship of the 1-D and 2-D MTF of the optical system, the sinusoidal targets are applied by use of Fourier transform.

At first, we analyze the 1-D MTF with a typical 1-D sinusoidal template which is shown in Fig. 1(a) and its expression is

$$I_{\text{input}}^{1-D} = \frac{1}{2} \left[ 1 + \sin(2\pi f) \right],$$

(2)

where $f$ is the spatial frequency, and $f = 1/(2a)$. If we treat the OSUT as a linear time-invariant system, then the input sinusoidal signal will be modulated by the system’s MTF when it transmits through the system, and the output signal will be

$$I_{\text{output}}^{1-D} = \frac{1}{2} \left[ 1 + \sin(2\pi f) \cdot \text{MTF}_{1-D}(f) \right],$$

$$= \frac{1}{2} \left[ 1 + \sin \left( \frac{\pi x}{a} \right) \cdot \text{MTF}_{1-D} \left( \frac{1}{2a} \right) \right],$$

(3)

where $\text{MTF}_{1-D}(f)$ is the 1-D MTF value at spatial frequency $f$.

The 2-D case is more complex than that of the 1-D. A typical 2-D sinusoidal target is shown in Fig. 1(b), which can be expressed as

$$I_{\text{input}}^{2-D} = \frac{1}{2} \left[ 1 + \sin(2\pi f_x) \cdot \sin(2\pi f_y) \right],$$

(4)

where $f_x$ and $f_y$ are the fundamental frequencies along the horizontal and vertical directions, and $f_x = f_y = 1/(2a)$. As for the 2-D target, we also need to obtain the output signals when input signals transmit through the optical system by analyzing its 2-D spectrum with 2-D Fourier transform, as in Eq. (5). Its spectrum is shown in Fig. 1.

$$H(\xi, \eta) = \frac{1}{2} \left\{ 1 + \frac{1}{4} \left[ \delta(\xi - f_x) - \delta(\xi + f_x) \right] \right\}$$

$$\cdot \left[ \delta(\eta + f_y) - \delta(\eta - f_y) \right]$$

$$= \frac{1}{2} \left\{ 1 + \frac{1}{4} \left[ \delta(\xi + f_x, \eta + f_y) + \delta(\xi + f_x, \eta + f_y) \right] - \delta(\xi + f_x, \eta - f_y) \right\}.$$

(5)

Equation (5) shows that 2-D target contains different frequency components in the 2-D frequency domain, and indicates the modulation features of the imaging system in the 2-D target case when adopting the 2-D MTF.

In Fig. 1, one can easily note that four different frequency components uniformly distribute on a circle whose radius is $f = (f_x^2 + f_y^2)^{1/2}$. In terms of an ideal axis symmetrical system (aberration-free), its 2-D MTF values will be equal to all the frequency points on the circle which can be calculated with equation

![Fig. 1 Typical sinusoidal targets: (a) one-dimensional (1-D) target, (b) two-dimensional (2-D) target.](https://www.spiedigitallibrary.org/journals/Optical-Engineering/article/104105-2/ downloaded_from=https://www.spiedigitallibrary.org/journals/Optical-Engineering/article/104105-2/ October 2014 • Vol. 53(10))
\[ MTF_{2-D}(f_x, f_y) = MTF_{1-D} \left( \sqrt{f_x^2 + f_y^2} \right), \]  
\[ MTF_{2-D}(f) = MTF_{1-D}^2 \left( \sqrt{2f} \right). \]

where \( MTF_{2-D}(f_x, f_y) \) is the 2-D MTF of the system at frequency \((f_x, f_y)\). Based on Eq. (6), the output signal of the system is

\[ I_{output}^{2-D} = \frac{1}{2} \left[ 1 + \sin(2\pi f_x a) \cdot \sin(2\pi f_y a) \cdot MTF_{2-D}(f_x, f_y) \right] \]

\[ = \frac{1}{2} \left[ 1 + \sin \left( \frac{\pi x}{a} \right) \cdot \sin \left( \frac{\pi y}{a} \right) \cdot MTF_{1-D} \left( \frac{\sqrt{2}}{2a} \right) \right]. \]  

(7)

If we focus the distribution on the horizontal direction \((\hat{x})\) at the center of a row, say \(y = a/2\), then Eq. (7) becomes

\[ I_{output}^{2-D} = \frac{1}{2} \left[ 1 + \sin \left( \frac{\pi x}{a} \right) \cdot MTF_{1-D} \left( \frac{\sqrt{2}}{2a} \right) \right]. \]  

(8)

Equations (7) and (8) give the two directions and the \((\hat{x})\) direction’s expressions, respectively, of the 2-D output of the system. By comparing Eq. (3) with Eq. (8), one can note that although both of them have the same input expression, they are modulated differently which leads to different outputs. As the image brightness of a 2-D target changes in two orthogonal directions and a 1-D target changes in only one direction, the brightness change in the \((\hat{y})\) direction of the 2-D output will influence the MTF result; this will not happen to the 1-D target when one analyzes the \((\hat{x})\) direction’s MTF with the output images. Actually, this interaction of two orthogonal directions is more in line with the actual situation as most systems are used in a 2-D imaging scene which has abundant spatial frequencies distributed in 2-D frequency domain. Therefore, to evaluate the true resolving power of imaging systems, one should apply 2-D targets and adopt 2-D MTF as they can provide comprehensive modulation information about the imaging system.

Moreover, in ideal systems (aberration-free), we build the relationship between the 1-D and the 2-D MTF theoretically, shown in Eq. (9), which is also true in the vertical direction \((\hat{y})\).

\[ \frac{MTF_{1-D} \left( \frac{\sqrt{2}}{2a} \right)}{MTF_{2-D}(f)} = \frac{f_{CF}^2}{f_{CF}^1}, \]  

where \(f_{CF}^{2-D}\) and \(f_{CF}^{1-D}\) are the cutoff frequencies of 2-D and 1-D MTF, respectively. This conclusion is made for the case of ideal systems. In the following sections, we will discuss the values of the experimental result.

### 2.2 Random Target Method and Noise Reduction Approach

As stated above, a 2-D target can provide comprehensive information for the 2-D MTF measurement of optical imaging systems in 2-D imaging scenes. However, a selective 2-D target will improve the measurement efficiency of the 2-D frequency. It is appropriate to use random images because, in addition to the advantages stated in Sec. 1, one can easily obtain its 2-D frequency spectrum through 2-D fast Fourier transform (FFT). A pixels random image is shown in Fig. 3 and its 1-D and 2-D PSD are shown in Figs. 4(a) and 4(b).

Random images are generated by a random number generator. Although a random target method is performed, a series of random images are displayed in a liquid crystal display (LCD) one by one which are imaged by the OSUT on a CCD. By calculating the ratio of the output image captured by the CCD to the input random image’s PSD, one can get the system’s MTF. The mathematical principle of this process could be described as

\[ PSD_{output} = \left[ MTF_{sys} \times MTF_{test} \right]^2 \times PSD_{input}, \]  

where output PSD and input PSD are the PSDs of the final images and the original images on the LCD. \(MTF_{sys}\) and
MTF_{test} are the system inherent MTF of the system devices (including LCD and CCD) and the OSUT. Here, to reduce the influence of temporal and spatial noises of the experimental setup, \( \text{PSD}_{\text{output}} \) is determined by

\[
\text{PSD}_{\text{output}} = \text{PSD}_{\text{captured}} - \text{PSD}_{\text{system}},
\]

where \( \text{PSD}_{\text{captured}} \) is the PSD value measured with random images in the screen, while \( \text{PSD}_{\text{system}} \) is the PSD value measured without random images in the screen.

In 1-D and 2-D MTF measurements, we should calculate the PSDs of the input and output images, respectively. Then, Eq. (11) becomes

\[
\text{PSD}_{1-D}^{\text{output}}(f) = \left[ \text{MTF}_{1-D}^{\text{sys}}(f) \cdot \text{MTF}_{1-D}^{\text{test}}(f) \right]^2 \cdot \text{PSD}_{1-D}^{\text{input}}(f),
\]

\[
\text{PSD}_{2-D}^{\text{output}}(\xi, \eta) = \left[ \text{MTF}_{2-D}^{\text{sys}}(\xi, \eta) \cdot \text{MTF}_{2-D}^{\text{test}}(\xi, \eta) \right]^2 \cdot \text{PSD}_{2-D}^{\text{input}}(\xi, \eta).
\]

1-D and 2-D PSD can be obtained by applying 1-D FFT and 2-D FFT to the images. At the same time, the noise reduction method is applied to obtain a smooth 1-D MTF curve and 2-D MTF surface by taking average of the FFT results for a large number of images. Equations (15) and (16) describe the calculation process in detail

\[
\text{PSD}_{1-D} = \frac{1}{M_1} \sum_{i=1}^{M_1} \{\text{abs}[\text{FFT}(A_i)]^2/N_1\},
\]

\[
\text{PSD}_{2-D} = \frac{1}{M_2} \sum_{j=1}^{M_2} \{\text{abs}[\text{FFT2}(B_j)]^2/N_2\},
\]

where \( A \) is a set of \( 1 \times N_1 \) vectors, and \( A_i \) means the \( i \)th vector, \( B \) is a set of \( N_2 \times N_2 \) matrices and \( B_j \) represents the \( j \)th matrix of \( B \). \( M_1 \) and \( M_2 \) are the numbers of vectors or matrices of \( A \) and \( B \) where abs is the function for obtaining an absolute value.

We also discuss the relationship between the variances and peak to peak values of \( \text{PSD}_{1-D} \) and \( \text{PSD}_{2-D} \), and the relationship between the variances and peak to peak values of \( \text{PSD}_{1-D} \) and \( \text{PSD}_{2-D} \), as are shown in Fig. 3. The variances are stable when increasing the number of vectors and matrices, which implies that \( M_1 = 1024 \) vectors and \( M_2 = 1024 \) matrices are sufficient for 1-D and 2-D MTF analysis. The average results of 1-D and 2-D PSD are shown in Figs. 4(a) and 4(b).

**3 Experiment and Results**

**3.1 Experimental Setup and Experimental Procedure**

The schematic diagram of the experimental setup is shown in Fig. 2. A host with two LCDs is adopted. Monitor 1 is used to show the interactive interfaces of applications and monitor 2 is used to present the random images. Thus the parameters are defined, e.g., \( l \) and \( d \) are the pixel size of the LCD and CCD, respectively, and \( M \) is the reduction ratio of the optical system.
According to the sampling theorem, to avoid aliasing effects one should ensure \( f_{\text{max}} < f_{\text{N}} \) since the highest spatial frequency of the LCD measured in the image plane is \( f_{\text{max}} = 1/(2 \times l \times M) \) and the Nyquist frequency of the CCD is \( f_{\text{N}} = 1/(2 \times d) \).

In our experiment, monitors 1 and 2 are Samsung SyncMaster E1920W LCDs whose pixel size is 0.2835 mm with a total of \( 1440 \times 900 \) pixels. The CCD placed in the image plane is a ¼ in. Sony ICX618 monochrome CCD. Its total number of pixels is \( 656 \times 492 \) with each pixel size being \( 5.6 \mu m \times 5.6 \mu m \). Therefore, according to the constraints, the optical system’s reduction ratio could not be smaller than 0.0197. In this paper, the reduction ratio of the OSUT is 0.02 and the highest frequency of the screen measured in the image plane is \( 1/(2 \times 0.2835 \times 0.02) \approx 88.2 \) cycles/mm.

The block diagram of the experiment is shown in Fig. 8. First of all, the CCD captures a series of images without random images displayed in the screen. Also, these captured images will be used to calculate the temporal and spatial noises (\( \text{PSD}_{\text{sys}} \)) of the experimental setup. Then, \( M_2 = 1024 \) random images are displayed on monitor 2 one by one. These \( N \times N \) random images are generated in MATLAB by using the functions named rand and imshow, and we set \( N = 256 \) here because it is precise enough for the measurement, see Ref. [3]. The original random image and the image captured by the CCD are saved in the host. Finally, all the images are used to calculate the 2-D PSD, i.e., \( \text{PSD}_{\text{measured}}^{\text{2-D}} \), and \( M_1 = (M_2/N) \) images of them are used to calculate the 1-D PSD, i.e., \( \text{PSD}_{\text{measured}}^{\text{1-D}} \). After acquiring these PSD values, we can calculate the values of the optical system’s 1-D and 2-D MTF based on Eqs. (13) and (14).

3.2 Results and Discussion

A random image on the screen and its image captured by the CCD are shown in Fig. 9. The 1-D MTF in the horizontal direction is shown in Fig. 10 and the 2-D MTF is shown in Fig. 11. The 1-D MTF and the curve of 2-D MTF in the (\( \hat{x} \)) direction are plotted in Fig. 12.

In Fig. 12, one can easily note that for a practical system, the 2-D MTF values are lower than the 1-D MTF values at every spatial frequency point. The 1-D MTF’s value is 0.023 at the cutoff frequency point. If we set 0.023 as the cutoff value, then the cutoff frequency of the 2-D MTF is 65.9 cycles/mm. Thus \( 88.2/65.9 = 1.34 \), which approximates \( \sqrt{2} \). These results are consistent with the conclusions for an ideal system.

According to Eq. (9), another curve, the ideal curve, is also illustrated in pink in Fig. 12. The value for the ideal

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**Fig. 6** Average results: (a) 1-D PSD averaged on 1024 vectors and (b) 2-D PSD averaged on 1024 matrices.

**Fig. 7** Schematic diagram of the experimental setup.

**Fig. 8** Block diagram of experimental procedures.
curve at frequency $f$ is equal to that of the 1-D MTF at frequency $\sqrt{2}f$. Also, when comparing with the 2-D MTF curve (in blue), these two curves do not strictly obey the relationship in Eq. (9) except at one point, which is located at about $0.38f_c \approx 33.47$ cycles/mm. The 2-D MTF curve will be lower than the ideal curve when $f < 0.38f_c$, and will be higher than it when $f > 0.38f_c$. These results are not completely consistent with the conclusions for an ideal system when considering various aberrations in the practical systems since these aberrations will be reflected in the 2-D MTF measurement results.

4 Conclusions

The relationship between 1-D and 2-D MTF has been discussed in theory and investigated in an experiment based on the random target method. The theoretical and experimental results show that the 2-D MTF’s values and cutoff frequency are lower than their counterparts in 1-D MTF, and that 2-D MTF can provide more comprehensive information.

Fig. 9 (a) Random image on the screen. (b) Image captured by the CCD.

Fig. 10 Raw data of 1-D MTF and curve fitted with polynomials.

Fig. 11 2-D MTF.

Fig. 12 The comparison of 1-D and 2-D MTF.
than the 1-D MTF does since it covers the 2-D frequency domain.

The major contributions of this work are that, to the best of our knowledge, we take the average of the 2-D FFT results of a sufficient number of random images; this is used as a noise reduction method in the 2-D MTF measurement of optical imaging systems for the first time. Also, we discuss the characteristics of 2-D MTF and 1-D MTF in terms of MTF values and cutoff frequency through comparing 2-D MTF with 1-D MTF in the same direction.

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References


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