Real-time display on Fourier domain optical coherence tomography system using a graphics processing unit

Yuuki Watanabe* and Toshiki Itagaki
Yamagata University, Graduate School of Science and Engineering, 4-3-16 Johnan, Yonezawa, Yamagata, 992-8510, Japan

Abstract. Fourier domain optical coherence tomography (FD-OCT) requires resampling of spectrally resolved depth information from wavelength to wave number, and the subsequent application of the inverse Fourier transform. The display rates of OCT images are much slower than the image acquisition rates due to processing speed limitations on most computers. We demonstrate a real-time display of processed OCT images using a linear-in-wavenumber (linear-k) spectrometer and a graphics processing unit (GPU). We use the linear-k spectrometer with the combination of a diffractive grating with 1200 lines/mm and a F2 equilateral prism in the 840-nm spectral region to avoid calculating the resampling process. The calculations of the fast Fourier transform (FFT) are accelerated by the GPU with many stream processors, which realizes highly parallel processing. A display rate of 27.9 frames/sec for processed images (2048 FFT size ×1000 lateral A-scans) is achieved in our OCT system using a line scan CCD camera operated at 27.9 kHz.

Keywords: optical coherence tomography; graphics processing unit.

Optical coherence tomography (OCT) is a noninvasive, noncontact imaging modality used to obtain cross sectional images of tissue structures with high resolution. Broadly, OCT has been classified into two categories: time-domain (TD)-OCT and Fourier-domain (FD)-OCT. Conventional TD-OCT can detect the echo time delays of light by measuring the interference signal as a function of time during a depth scan (A-scan) in a reference arm at each position of a lateral probe beam. In FD-OCT, instead of a mechanical A-scan, depth information can be retrieved by detecting the interference signal as a function of wavelength. In spectral-domain (SD) OCT, this is achieved with a broadband source and a spectrometer on the detector arm. Optical frequency domain imaging (OFDI) uses a swept source and point detector to acquire the same information. The main advantage of these schemes over TD-OCT is a marked increase in sensitivity and imaging speed. Spectrometers with a linear array detector and swept source normally operate at tens of kHz, which allows data acquisitions at video rates [30 frames/sec, (fps)]. FD-OCT images require resampling of the axial data from wavelength (λ) space to wavenumber (k=2π/λ) space, and the subsequent application of the inverse Fourier transform. Therefore, although data acquisitions of high-speed FD-OCT are achieved at a higher rate than that of video, the display rate of OCT images often occurs at a much slower rate than the acquisition, because this heavy signal processing must be performed by a computer.

One example of real-time display has been demonstrated by digital signal processing (DSP) hardware using a single field programmable gate array (FPGA) integrated circuit (IC) and a custom electronics board. The display rate for processed OCT images (1024 axial pixels×512 lateral A-scans) was 27 fps in the SD-OCT system. This type of equipment is expensive, and must be custom built for FPGA technology.

To avoid calculating a numerical k-space resampling prior to Fourier transform, a linear-in-wave-number (linear-k) spectrometer and k-space linear swept source have been designed. A linear-k spectrometer consisting of a grating and an optical glass prism in the 1.3-μm region not only saved computing time but also improved SNR falloff. The FD-OCT systems based on linear-k techniques still require high speed fast Fourier transform (FFT) processing to realize real-time display of OCT images.

Recently, one approach to accelerating numerical calculations has been to use a graphics processing unit (GPU) instead of a central processing unit (CPU). A GPU with many stream processors allows us to use highly parallel processors. The advantage of GPU computing is the implementation of high speed computation at a low cost, and simple programming on the host computer. In the field of optics, GPU techniques have been applied to reconstruct digital holograms.

In this work, we demonstrated real-time display on a linear-k SD OCT system using GPU programming. We estimated the optimal combination of a diffractive grating and a prism for the linear-k spectrometer in the 840-nm spectral region. The computing time using the GPU was 6.1 ms for data size of 2048 FFT size ×1000 lateral A-scans, and was shorter than the frame interval time (35.8 ms) using a line scan camera at 27.9 kHz. A display rate of 27.9 fps for pro-

Fig. 1 Schematic of spectral domain optical coherence tomography with a linear-in-wave-number spectrometer. SLD, superluminescent diode; BS, beamsplitter; L, achromatic lens; εd, diffraction angle; θa, incident angle; θo, output angle of prism; α, apex angle of prism; β, angle between grating and prism; x0, central location of CCD camera.
cessed images was achieved using a low cost GPU.

Figure 1 shows a schematic of our SD-OCT system. The output light of a superluminescent diode [SLD-370-HP, Superlum, (County Cork, Ireland), center wavelength $\lambda_0=840.8$ nm, full-width at half-maximum spectral width $\Delta\lambda=48.7$ nm] was split into a sample and reference arm, with the latter terminated by a mirror. A probe at the end of the sample arm delivered light to a sample and received backscattered light from within the sample. Achromatic lenses ($f$ =100 mm) were inserted in both arms. The predicted lateral resolution was 21.4 $\mu$m. The light returned from the two interferometer arms was recombined and directed to a linear-$k$ spectrometer consisting of a diffraction grating (Wasatch Photonics, Volume Phase Holographic Grating, 1200 lines/mm) and an optical glass prism. When the incident angle is the blaze angle, $\theta_0 = \sin^{-1}(m\lambda_0/2)$, which gives the best diffraction efficiency, the first-order diffraction angle of light at a wavelength $\lambda$ is

$$\theta_d(\lambda) = \sin^{-1}(m\lambda - \sin \theta_0) = \sin^{-1}(m\lambda - m\lambda_0/2),$$

where $m$ is the groove number of the grating. The output angle $\theta_{out}$ of the prism is

$$\sin \theta_{out}(\lambda) = n(\lambda) \sin \left\{ \alpha - \sin^{-1} \left[ \frac{\theta_d(\lambda) + \beta}{n(\lambda)} \right] \right\},$$

where $n(\lambda)$ is the refractive index determined by the material. The parameters $\alpha$ and $\beta$ are the apex angle of the prism and the angle between the grating and the prism, respectively. The light from the prism was focused on a line scan CCD camera (e2v Aviiva SM2, 2048 pixels, 14-$\mu$m pixel size, 12-bit resolution) using an achromatic lens ($f$=250 mm). The location of the spectral component at the CCD camera is described as

$$x = f \cdot \tan(\theta_{out}(\lambda) - \theta_0) + x_0,$$

where $\theta_0$ is the output angle of the light at the central location $x_0$. The output of the camera was transferred to a personal computer (PC) via a camera link board (National Instruments, Austin, Texas, PCIe-1427, 16-bit resolution). The sampled data were transferred to a GPU on a graphics card [Nvidia (Santa Clara, California) GeForce GTX 280, processor clock of 1296 MHz, memory clock of 2214 MHz, 240 stream processors, and memory 1 Gbytes]. We used Nvidia’s compute unified device architecture (CUDA) which could be programmed in only a C language environment to implement the processing power of the GPUs. We developed software that included image acquisition, GPU programming, and a graphical user interface environment in Microsoft Visual C++, 2008 Express Edition.

First we calculated the location of the spectral component at the focal plane in a wave number range between 7 and 8 ($/\mu$m) at each angle $\beta$ between the prism and the grating to optimize the linearity of the spectrometer. Here, the prism materials are BK7, F2, and SF10, with the angle $\alpha=60$ deg. A comparison of the derivatives of the locations at the optimal angle with respect to wavenumber is shown in Fig. 2(a). The optimal angle was estimated by the standard deviation of the derivatives, as shown in Fig. 2(b). From these, the combination of the grating with 1200 lines/mm and the F2 equilateral prism were suitable for the linear-$k$ spectrometer.
Govindaraju et al. have compared their novel algorithms of discrete Fourier transforms to CUFFT for the GPU and MKL on the CPU. Their algorithm was two times faster than the CUFFT on the GPU (Nvidia, GTX280) and 12 times faster than the MKL on the CPU (Intel QX9650 3.0-GHz quad-core processor and 4-GB memory) for computing the data size of 2048 FFT size × 4096 number of FFTs. From this comparison, we can understand that the CUFFT on the GPU was about six times faster than the MKL on the CPU.

Finally, we measured the OCT images of a human finger pad in vivo. We used a commercial available F2 prism (Thorlabs Incorporated, Newton, New Jersey) for the linear-k spectrometer. The spectrometer settings provided a spectral resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm. With a probing power of 5.0 mW and an integration time of 34 μs, a sensitivity of 99 dB was measured close to the zero delay and a resolution of 0.049 nm and a depth range of 3.6 mm.

In conclusion, we demonstrate a real-time display on the linear-k SD OCT system using GPU programming. We use the linear-k spectrometer combined with a diffractive grating (1200 lines/mm) and a F2 equalateral prism at 840 nm to avoid resampling of the axial data from wavelength to wave number. The calculation of the FFT is accelerated by the GPU. The computing time is 6.1 ms for data of size 2048 pixels × 1000 lateral A-scans, and is shorter than the frame interval time of the interference frame. Our system can display processed OCT images in real time at 27.9 fps. Since the GPUs are cost effective for real-time display of FD-OCT images, the potential applications for this technique are wide.

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