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Abstract. The use of optical tweezers (OTs) and spin angular momentum transfer to birefringent particles allows new mechanical measurements in systems where torque and rotation are relevant parameters at the single-molecule level. There is a growing interest in developing simple, fast, and inexpensive protocols to produce a large number of submicron scale cylinders of quartz, a positive uniaxial birefringent crystal, to be employed for such angular measurements in OTs. Here, we show that laser interference lithography, a method well known for its simplicity, fulfills these requirements and produces quartz cylindrical particles that we successfully use to apply and measure optical torque in the piconewton nm range in an optical torque wrench. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: [10.1117/1.JMM.15.3.034507](https://doi.org/10.1117/1.JMM.15.3.034507)]

Keywords: nanofabrication; laser interference lithography; optical tweezers; torque spectroscopy; single-molecule biophysics.

Paper 16082 received May 31, 2016; accepted for publication Aug. 23, 2016; published online Sep. 8, 2016.

1 Introduction

In the last few decades, several technical breakthroughs have provided researchers with the ability to apply an external “force” to a microscopic particle in the piconewton range while measuring its position with subnanometer resolution. Since their development,¹ optical tweezers (OTs) have been of great interest for their all-optical manipulation capabilities and have proven their potential in several different applications in physics as well as in biology.² In particular, together with atomic force microscopes and magnetic tweezers,³ OTs are routinely used to study biological systems at the single-molecule level. The mechanical behavior of single biopolymers, such as DNA and the mechanochemical properties of enzymes and molecular motors can be directly probed with OT by optical forces. This is achieved by biochemically tethering the optically trapped particle, often a microbead, to the biological system under study. Using the trapped particle as a handle, force can be detected from and transferred to the molecular system.

There is a growing interest in expanding the capabilities of optical manipulation by controlling and measuring the “torque” on the trapped particle.⁴ Several biological molecular systems are susceptible to torque and twist, parameters that are often finely controlled by living cells. Typical examples include the degree of coiling of the double-stranded DNA molecule (modified by specialized enzymes), ATP synthesis (accomplished by a rotary machine in mitochondria), and motility in many bacteria (based on a rotary motor).⁵ Therefore, the development of techniques that allow angular manipulation will open new methods of studying biological

nanoscale systems, where rotation is a relevant physical parameter.

In the angular OT implementation we employ, further termed optical torque wrench (OTW),^{6–8} a microscopic birefringent particle is optically trapped and angularly manipulated using the linear polarization of the laser. The particles, nanofabricated and removed from a quartz wafer, are shaped as cylinders with an aspect ratio of ~ 3 , a geometry that conveniently fixes the geometrical axis of the cylinder in the optical trap parallel to the laser propagation direction.⁹ Different protocols have been used for the fabrication of such birefringent particles. The first demonstrations of angular manipulation in OT employed irregularly shaped microcrystals,^{6,10} or asymmetric dielectric particles.¹¹ Later, the advantages of the cylindrical geometry of a uniaxial-positive material were demonstrated.¹² Protocols based on optical and electron beam lithography^{7,12,13} have been successfully used, while recently, a simpler fabrication process based on nanosphere lithography has been developed.¹⁴ However, the complexity of the fabrication techniques remains an obstacle for a more widespread use of angular manipulation in OT.

Here, we propose to use a method of fabricating quartz cylinders based on laser interference lithography (LIL), a well-known, simple, fast, and inexpensive technique, which produces submicron particles suitable for optical angular manipulation and torque measurement.

2 Methods

2.1 Laser Interference Lithography

LIL, also known as holographic lithography, consists of the direct transfer of laser interference patterns on a photoresist, without the need of a lithography mask [Fig. 1(a)]. LIL combines the ease and speed of a direct illumination in a simple optical setup for applications, where large area ($\sim \text{cm}^2$)

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Fig. 1 Scheme of LIL. (a) Scheme of the optical setup employed to produce the interference fringes. (b) Result of the sum of two interference patterns. (c) Interference patterns generated by two light beams intersecting at an angle θ . (d) Schematic view of the aspect ratio of the exposed photoresist as a function of exposure.

patterns of lines or dots are needed,^{15,16} as in our case [Fig. 1(b)]. The linear interference pattern resulting from the coincidence of two plane wavefronts has a spatial period given by

$$\Lambda = \frac{\lambda}{2 \sin(\theta/2)}, \quad (1)$$

where λ is the wavelength of the laser source and θ is the angle between the two beams [Fig. 1(c)]. By increasing the number of interfering light beams, it is possible to create more complex interference patterns such as arrays of dots in two or three dimensions.¹⁷ Here, we simply use two consecutive illuminations, superposing two linear interference patterns oriented at 90 deg to one another.

The optical setup used in our experiments is depicted in Fig. 1(a). A 30-mW laser with $\lambda = 405$ nm produces a Gaussian beam, which is focused on a 10 μm wide pinhole, resulting in a coherent light beam propagating from the aperture with a coherence length larger than 10 m. The divergent beam strikes two adjacent mirrors oriented at an angle θ , creating two beams interfering at the plane where the sample, coated with photoresist, is placed. This interference region is about 3 cm $\times$ 3 cm in our setup and the illuminance is 0.16 mW cm⁻², which imposes minute-long exposures for common photoresists. By adjusting the angle θ between the two mirrors, according to Eq. (1), we can continuously tune the spatial period of the interference and generate patterns with a pitch from 400 nm up to 2 μm . The exposure duration is set to provide the required optical dose to completely cross-link the photoresist at the location of constructive interference. By controlling the exposure time, it is also possible to tune the ratio of exposed versus nonexposed photoresist and hence, to adjust the lines width or dots diameter while keeping a constant pitch [Fig. 1(d)].

2.2 Optical Torque Wrench

Depending on their spin, photons carry positive or negative angular momentum, which corresponds to the two left- and

right-circular polarization components. Because of the birefringence, the polarization state of the trapping beam is modified during the propagation through the particle trapped in the laser focus. This results in a change in the total spin angular momentum of the laser beam, which reflects the torque transferred to the particle. The induced dipole moment $\vec{P}$ and the laser electric field $\vec{E}$ are generally not parallel in the birefringent crystal. The angle between the two vectors results in a restoring torque $\vec{\tau} = \vec{E} \times \vec{P}$ on the particle.⁶ As a consequence, the extraordinary axis of the quartz cylinder tends to orient parallel to the linear polarization of the laser. The optical torque transferred to the particle can be written as

$$\tau = \tau_0 \sin(2x), \quad (2)$$

where x is the angle between the laser polarization and the extraordinary axis of the cylinder and τ_0 is the maximum torque (a function of laser intensity, particle geometry, and birefringence).¹⁰

Our optical setup is described in detail in Refs. 8 and 18. Briefly, the trap consists of an infrared laser ($\lambda = 1064$ nm, 100-mW CW at the optical trap, TEM₀₀) focused by a large numerical aperture objective (NA = 1.2) in a flow cell containing cylinders dispersed in water. The orientation of the linear polarization of the laser is dynamically controlled by an electro-optical modulator (EOM) combined with a quarter waveplate.^{7,8} In our experiments, we control the frequency ω of rotation of the linear polarization by driving the EOM with a sawtooth voltage signal of variable frequency. The polarization can be set in rotation in both directions with ω in the range from 0 to few kHz.

The transferred torque is measured by analyzing the imbalance of the circular components of the polarization at the output of the trap with respect to the input. After calibration of the angular trap,¹⁸ absolute measurements of torque are performed at 20-kHz sampling rate.

3 Results

3.1 Quartz Microcylinders Fabrication

We depict the microfabrication process in Fig. 2. First, a chromium layer of 30 nm is sputtered onto a $24 \times 24 \text{ nm}^2$ single-crystal quartz substrate (X-cut), previously cleaned with a Piranha solution. Second, we spin-coat a thin layer of AZ 701 MIR photoresist (Merck Performance Materials GmbH) at 4000 rpm for 30 s, followed by soft baking at 95°C for 1 min. The photoresist is diluted (2:1) to achieve a final thickness of 600 nm. The quartz sample is then exposed on the LIL setup, prepared for a fixed interference period (typically $1 \mu\text{m}$). Exposure is made in two steps of 130 s each, rotating the sample by 90° in the interference plane. After exposure, the sample is postbaked at 110°C for 1 min and developed with AZ 726 developer for 17 s under smooth agitation. Figures 3(a) and 3(b) show two SEM images of lines and dots arrays obtained after development. The next step consists in transferring the photoresist pattern onto the quartz substrate. To achieve the high anisotropy required by the cylindrical geometry, we use inductive coupled plasma reactive ion etching (ICP-RIE). To improve the selectivity of the technique (which is low especially when using photoresists), the key is to use a hard mask, as a chromium layer, and a two-step ICP-RIE process, as described below. Hard masks are often used in plasma etching, in particular to prevent photoresist shrinking,¹⁹ and the materials employed include Ni, Al, or ZnO. Abe and Esashi²⁰ reported the etching of $90\text{-}\mu\text{m}$ deep quartz trenches by using a $4\text{-}\mu\text{m}$ Ni metal mask with SF_6 , SF_6/Ar , and SF_6/Xe RIE gas plasma. Also, a SU8 thick photoresist has been used as a hard mask for quartz etching.²¹ In our case, we find that the submicron dimensions of the quartz cylinders require a thin (30 nm) hard mask layer. Following LIL patterning, the chromium layer is etched with an Ar plasma in the absence of oxygen, using a Corial 250D ICP RIE (200 W RF and 400 W LF). The absence of oxygen prevents the photoresist from shrinking during etching, allowing the unprotected hard mask to be completely removed in 6 min with sufficient selectivity. Etching of quartz is achieved by a second ICP-RIE process, using a mixture of CHF_3 (200 sccm) and O_2 (100 sccm), an internal pressure of 1.2 mTorr, and

Fig. 2 Steps of the microfabrication process: (a) initial stack, photoresist on a 30-nm chromium layer on quartz substrate, (b) LIL and development of the photoresist, plasma sputter etching of chromium, (c) plasma etching of quartz, and (d) cleavage by microtome blade.

Fig. 3 (a) and (b) SEM pictures of the photoresist patterns obtained by LIL: (a) lines with 800 nm pitch. (b) Dots with $1\text{-}\mu\text{m}$ pitch. (c) SEM image of ICP-RIE etched quartz cylinders (45-deg tilt). (d) SEM image of cylinders mechanically cleaved from the substrate.

incoming power of 200 W RF and 800 W LF. In these conditions, the etching rate of quartz is about 100 nm/min .

The cylinders obtained are slightly conical, with a wall angle of about 80° [Fig. 3(c)]. Aiming at an aspect ratio of ~ 3 , we can adjust the etching time to produce cylinders with heights ranging from 900 nm to $1.6 \mu\text{m}$, with a homogeneity across the sample of 3% to 5%. After etching, the cylinders are mechanically cleaved and removed from the substrate by using a microtome blade, as can be observed in Fig. 3(d). They are finally collected and stored in water (a surfactant can be used to avoid coalescence). Before cleavage, the top surface of the pillars can be specifically functionalized.¹³ Given the dimensions of the wafer ($2 \times 2 \text{ cm}^2$) and the pitch of the structures ($1 \mu\text{m}$), the production of $\approx 4 \times 10^8$ cylinders would be expected. However, irregularities in the thickness of the photoresist near the edges of the substrate decrease the efficiency of the process from 60% to 70% of the total area. The distribution of sizes obtained for the cleaved cylinders, shown in Fig. 3(d), is summarized in Table 1.

3.2 Optical Torque Measurement on a Trapped Birefringent Cylinder

In Fig. 4, we show the dynamical measurements of the transferred torque on a single cylinder in the optical trap [sketched in Fig. 4(a)], performed for different frequencies of rotation

Table 1 Cylinder size statistics for the $1\text{-}\mu\text{m}$ period series shown in Fig. 3(d) ($N = 35$).

Dimensions (nm)	Mean	Standard deviation
Upper diameter	330	40
Lower diameter	490	50
Height	1400	60

Fig. 4 Torque measurements on a trapped cylinder. (a) Sketch of the cylinder in the optical trap: at equilibrium, the geometrical axis of the cylinder is parallel to laser propagation direction. The extraordinary axis of the crystal χ_e and the polarization of the laser P are shown. (b) Average torque transferred to the particle as a function of the polarization rotation frequency ω . Laser power = 55 mW (blue), 92 mW (orange). (c)–(e) The instantaneous torque traces recorded at the indicated values of ω , as shown also in (b).

ω of the linear polarization of the laser at the optical trap. As predicted by Eq. (2), when the linear polarization rotates at a frequency ω , the dynamical response of the system is “excitable” and can be well described by the one-dimensional motion of a particle along a tilted periodic potential.^{8,18} For low ω , the extraordinary axis of the cylinder follows the polarization rotation in phase. In this regime, the average optical torque transferred to the particle is linearly proportional to ω , as seen in Fig. 4(b). The time resolved torque traces are characteristic of confined Brownian motion of an angularly trapped particle, as shown in Fig. 4(c). When ω reaches the critical value $\omega_c = \tau_o/\gamma$ (with τ_o given in Eq. (2) and γ the angular drag coefficient of the cylinder), the cylinder cannot follow in phase the rotation of the polarization. In this regime, thermal noise triggers stochastic escape events of the particle axis from the potential created by the rotating laser polarization. The average torque transferred to the particle decreases with increasing ω [Fig. 4(b)], and the escape events are apparent as spikes in the torque

signal [Fig. 4(d)]. For larger ω , the rotation of the polarization is too fast to allow the particle to follow it in phase, and the average torque falls to zero [Fig. 4(b)]. The cylinder axis remains quasistatic in the trap, leading to a quasiperiodic torque trace [Fig. 4(e)]. The calibration of the optical signal allows absolute measurements of torque in physical units (pN nm) and provides a value for the angular drag coefficient γ of the particle immersed in water.¹⁸ Trapping one cylinder from the batch shown in Fig. 3(d), whose dimensions are distributed as indicated in Table 1, the calibration yields a value of γ of 1.1 ± 0.2 pN nm s. This is compatible with the theoretical value of 0.9 pN nm s for a cylinder with the same dimensions.²² This dynamical behavior of the trapped cylinder, well described by the model, confirms that optical torque in the range of pN nm, relevant in single-molecule essays, can be transferred and measured on these birefringent cylinders trapped in an OTW.

4 Conclusions

We have presented a simple protocol based on LIL for the fabrication of quartz cylindrical particles suitable for transfer and measurement of torque in single-molecule optical manipulation essays. Based on a simple and compact optical setup, the interference-based exposure, parallel and noncontact in nature, is very well suited for the submicron cylindrical geometry required. This reduces substantially the complexity, time, and cost of the fabrication of birefringent particles used in angular measurements in optical tweezers.

Acknowledgments

We are grateful to A. Nord for critical reading of the manuscript. We acknowledge funding from the European Research Council under the European Union’s Seventh Framework Programme (FP/2007-2013)/ERC Grant Agreement no. 306475.

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