Phase-contrast microscopy by in-line phase-shifting digital holography: shape measurement of a titanium pattern with nanometer axial resolution

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Abstract. Precision phase-contrast imaging has been achieved with in-line phase-shifting digital holographic microscopy. The complex amplitude of the object field on the charge-coupled device plane is measured by the phase-shifting method with a self-calibration algorithm, and the magnified object image is reconstructed with a plane wave expansion method. The phase fluctuation in the blank image without sample is 1.30 deg and the three-dimensional shape of a titanium phase test pattern is measured with an accuracy of 5.51 nm (corresponding to the phase resolution of 3.63 deg), which are better than those of off-axis systems.

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Three-dimensional shape measurement of microscopic objects is an important task in many fields such as biology, microelectronics, and microelectromechanical systems engineering. Scanning confocal microscopy has been used for this purpose, but the process of the three-dimensional scanning is rather time-consuming.¹ Microscopic electronic speckle pattern interferometry can provide the three-dimensional information with a whole-field measurement, but it requires a focusing mechanism to record speckle patterns at various field depths.²

In digital holography, many holograms can be recorded with a charge-coupled device (CCD) in subseconds, and the images of the object are reconstructed numerically afterward. Because the focusing can be adjusted in the reconstruction process, digital holography is free from the process of mechanical focusing and can be used to monitor the dynamic change of objects.

A digital holographic system can be configured in off-axis or in-line setups. In case of a typical in-line setup, the reconstructed object image is overlapped with the zero-order and the twin images. Although this problem can be solved with an off-axis setup, there is a drawback: about a half of the CCD pixels are filled with the carrier fringes and the distance between the object and the CCD must be long enough to separate the object image from the zero-order image. As a result, the numerical aperture of the imaging

optics is reduced, and the obtained image is of low resolution. The best phase resolution achieved so far is 2 to 4 deg on the blank image without any sample^{3,4} and about 10 deg in the flat area of the sample.⁵

The complex object field on the CCD plane can be measured in an in-line digital holographic system using the phase-shifting method.^{6–8} The object image reconstructed from this complex field is free from zero-order and the twin images and can have better phase resolution than can be obtained with an off-axis system. Therefore, an in-line phase-shifting digital holography system can be more useful in the precision shape measurement of transparent objects whose thickness or height profiles are proportional to the phase profiles of their complex images.^{4,5,9,10}

In this letter, very precise phase-contrast imaging using in-line phase-shifting digital holographic microscopy is reported. The three-dimensional shape of a titanium phase test pattern was measured with the phase fluctuation of 1.30 deg without a sample and 3.63 deg with a sample, corresponding to about 5.51-nm resolution. Both phase resolutions are better than those obtained with off-axis systems so far.^{3–5}

The schematic of our in-line phase-shifting digital holographic microscopy system is shown in Fig. 1(a). A linearly polarized He-Ne laser (10 mW, 632.8 nm) beam is collimated and divided into the object and the reference beams. An optical microscope (Zeiss Axiostar) is inserted in the object arm of the Mach-Zehnder interferometer. The collimated object beam enters through the microscope illumination port. The reference beam is reflected from a mirror attached to a piezoelectric transducer (PZT) controlled with a computer for phase shifting. Samples are observed through a 10×, 0.25-numerical aperture microscope objective. The object and the reference beams are combined by a beamsplitter placed in front of a CCD camera (Kodak MEGAPLUS 1.0/MV, 1008×1018 pixels, 9-μm×9-μm pixel size, 8 bits). The full field of view of the system with the 10× objective lens is 900 μm×900 μm.

A phase test pattern similar to the USAF1951 resolution-test pattern, as shown in Fig. 1(d), was made to test the phase resolution of our system. The size of bars in the largest group is 16.0 μm×80.0 μm, and the gap between them is of the same size. The second largest group is as large as 90% of the largest, and the group sizes are reduced similarly until the smallest bar becomes 6.20 μm×31.0 μm. About 10 nm of titanium was deposited on a 5-mm×5-mm sapphire substrate with 0.2-mm thickness by electron-beam evaporation method. The sapphire substrate had antireflection coatings on both surfaces to reduce the multiple reflections. Negative electron beam resistor (ER) was coated on the Ti layer, and ten groups of test patterns were written with a scanning electron microscope. After developing the negative ER, Ti was milled with an argon ion milling machine for a few minutes. Remaining negative ER was burned by oxygen plasma.

The three-dimensional shape of the Ti phase test pattern was measured by comparing the complex object fields on the sample plane reconstructed numerically from the complex object fields on the CCD plane with and without the test pattern in the object path. Four phase-shifted holograms of the flat area near the pattern were acquired. One of them is shown in Fig. 1(b). Their intensity distributions are given by

Fig. 1 (a) In-line phase-shifting digital holographic microscopy setup: SF, spatial filter; BS, beamsplitter; M, mirror; PZT-M, PZT-attached mirror; MO, microscope objective. Inset, prepared sample: S, sapphire substrate; T, titanium pattern. (b, c) Phase-shifted holograms on the CCD plane without and with the test pattern. (d, e) Amplitude and phase images of the test pattern.

$$I_n(x, y) = I_o(x, y) + I_r(x, y) + 2\sqrt{I_o(x, y)I_r(x, y)} \cos[\theta(x, y) + n\delta], \quad n = 0, 1, 2, 3. \quad (1)$$

In Eq. (1), $I_o(x, y)$ is the object beam intensity; $I_r(x, y)$ is the reference beam intensity; and $\theta(x, y)$ is the initial phase difference between the object and the reference beams. δ is the step size of the phase shift controlled with the PZT mirror and equals about $\pi/2$. It does not need to be exactly $\pi/2$, because the error can be corrected with a self-calibration algorithm.¹¹ $\theta(x, y)$ and the complex object field on the CCD plane, $U_o(x, y) = \sqrt{I_o(x, y)} \exp[i\theta(x, y)]$, is obtained by using the same algorithm. Four more holograms were captured after moving the Ti test pattern into the measurement area. One of them is in Fig. 1(c). The complex amplitude on the CCD plane, $U_s(x, y)$

Fig. 2 (a) Phase variation of the blank image obtained without the test pattern. Standard deviation is 1.30 deg. (b) Phase variation along the horizontal line in Fig. 1(e). Standard deviation is 2.73 deg. (c, d) Height profiles of the test pattern along the horizontal and vertical dotted line in the square marked in Fig. 1(e). (e) Three-dimensional shape of the test pattern in the square area marked in Fig. 1(e). (f) Three-dimensional shape of the smallest pattern in Fig. 1(e).

$= \sqrt{I'_o(x, y)} \exp\{i[\varphi(x, y) + \theta(x, y)]\}$ with the test pattern inserted was obtained similarly to how $U_o(x, y)$ was obtained. $I'_o(x, y)$ is the object beam intensity, and the additional phase $\varphi(x, y)$ is due to the test pattern.

The object field on the plane corresponding to the top of the test pattern, $U_s(X, Y, Z)$, was reconstructed from $U_s(x, y)$ using the plane wave expansion method devised in Ref. 12. We chose the plane wave expansion method, also known as angular spectrum method,¹³ because there is no restriction on the reconstruction distance. The object field on any reconstruction plane parallel to the hologram plane can be obtained from the following transformation of the object field on the hologram plane:

$$U(X, Y, Z) = F_{\perp}^{-1}\{F_{\perp}[U(x, y)]\exp[ik_z z]\}. \quad (2)$$

The value of Z that made the reconstructed amplitude image of the test pattern, $U_s(X, Y, Z)$, sharpest was used as the proper distance from the CCD plane to the object plane. The object field on the same plane without the pattern, $U_o(X, Y, Z)$, was reconstructed from $U_o(x, y)$ by the same method. The reconstructed amplitude image is shown in Fig. 1(d). The Ti pattern looks dark due to the attenuation of light by titanium. Figure 1(e) is the phase image of the test pattern obtained by unwrapping the phase difference of $U_o(X, Y, Z)$ and $U_s(X, Y, Z)$.

The phase fluctuation of the blank phase image obtained without any sample inserted in the object beam path was measured to check the lower bound of the phase measurement precision. The phase variation along a 1000-pixel-long line is shown in degrees in Fig. 2(a), whose standard deviation is 1.30 deg. The phase noise increases if a test object is inserted in the object beam path for many reasons

such as the multiple reflections between the optical surfaces and the scattering by the dust particles on the sample surface. The phase variation along the 450- μm -long horizontal dotted line marked in Fig. 1(e), which is in the plateau of the phase image of the test pattern, is shown in Fig. 2(b). Its standard deviation is 2.73 deg.

The interference fringes due to the multiple reflections are not noticeable in the area where titanium is not deposited, but they can be seen on the titanium pattern. It is because the surfaces of the substrate are antireflection coated whereas the titanium surfaces are not. As a result of these multiple reflections, the phase fluctuation on the titanium pattern is increased to 3.63 deg instead of 2.73 deg.

The profile of the Ti test pattern height, $l(X, Y)$, can be obtained from the relation

$$\alpha(X, Y) = (n_{Ti} - n_{air})kl(X, Y), \quad (3)$$

where $\alpha(X, Y)$ is the unwrapped phase difference between $U_s(X, Y, Z)$ and $U_0(X, Y, Z)$ plotted in Fig. 1(e). $n_{Ti}(=2.16)$ and $n_{air}(=1.00)$ are the refractive indices of titanium and air.

The height profile of a titanium bar pattern, along the horizontal dotted line in the square marked in Fig. 1(e), is shown in Fig. 2(c). As mentioned above, the multiple reflections increased the height fluctuation to 5.51 nm corresponding to 3.63 deg of phase variation. The height profile of the three-titanium-bar pattern, along the vertical dotted line in the square marked in Fig. 1(e), is shown in Fig. 2(d). The decreased height fluctuation on the substrate compared to the Ti pattern is due to the reduced multiple reflections on the substrate by antireflection coatings.

The three-dimensional shapes of the titanium test patterns in the square and in the rectangle marked in Fig. 1(e) are shown in Figs. 2(e) and 2(f). The average height of the titanium area is 7.82 nm. It can be seen that even the smallest bar group of the test pattern has been made close to the design value of 6.20- μm (width) $\times$ 31.0- μm (length) $\times$ 10-nm (height) bar size.

In summary, we have developed a precision in-line phase-shifting digital holographic microscopic system. The use of an in-line configuration made it possible to estimate the complex object fields on the CCD plane by the phase-shifting method. A self-calibration algorithm was used to enhance the phase accuracy by eliminating the phase-shift error. The complex object fields on the sample plane reconstructed numerically from the complex object fields on the

CCD plane has a higher phase resolution (1.30 deg) than could be obtained with off-axis digital holographic systems so far. The three-dimensional shape of a titanium phase test pattern was measured. The phase fluctuation level was increased to 2.73 deg in the flat area of the test pattern and to 3.63 deg in the titanium deposited area (corresponding to 5.51 nm of titanium thickness) due to the multiple reflections of the laser light. This system can be applied to the precision three-dimensional shape measurement of transparent microscopic objects with nanometer thicknesses.

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