Review of nonlinear ultrasonic guided wave nondestructive evaluation: theory, numerics, and experiments

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Abstract. Interest in using the higher harmonic generation of ultrasonic guided wave modes for nondestructive evaluation continues to grow tremendously as the understanding of nonlinear guided wave propagation has enabled further analysis. The combination of the attractive properties of guided waves with the attractive properties of higher harmonic generation provides a very unique potential for characterization of incipient damage, particularly in plate and shell structures. Guided waves can propagate relatively long distances, provide access to hidden structural components, have various displacement polarizations, and provide many opportunities for mode conversions due to their multimode character. Moreover, higher harmonic generation is sensitive to changing aspects of the microstructures such as to the dislocation density, precipitates, inclusions, and voids. We review the recent advances in the theory of nonlinear guided waves, as well as the numerical simulations and experiments that demonstrate their utility. © 2015 Society of Photo-Optical Instrumentation Engineers (SPIE) [DOI: 10.1117/1.OE.55.1.011002]

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1 Introduction

Nonlinear ultrasonic nondestructive evaluation uses interrogation signals at frequencies other than the excitation frequency to detect changes in structural integrity and characterize degradation of materials. Nonlinear ultrasonic methodologies provide improved sensitivity to damage and the ability to identify incipient damage relative to linear methods. In general, linear ultrasonic methods provide good sensitivity to macroscale damage such as long fatigue cracks. However, in many cases, once damage appears at the macroscale, the remaining life is short, severely limiting maintenance decisions. Thus, characterization of incipient damage could facilitate a paradigm shift in operations of structural systems from schedule-based to condition-based maintenance that would ultimately enhance safety and reduce life cycle costs. Nonlinear ultrasonics is a broad discipline1,2 which encompasses many specialized techniques reliant upon nonlinear material behavior to detect and/or characterize incipient damage. Some of these include nonlinear resonant ultrasound spectroscopy,3 nonlinear elastic wave spectroscopy,4–6 and second-harmonic generation.7 Modeling relies upon both classical and nonclassical8 nonlinear effects such as hysteresis. Early investigations focused on using higher harmonic generation for characterizing material microstructure.9–11 The contributions of elastic nonlinearity and dislocations were examined for bulk waves.12–14 Many studies over the years have employed second-harmonic generation to characterize microstructural changes, for example, associated with fatigue, creep, or thermal aging. A recent article15 provides a thorough review of second-harmonic generation measurements. The overwhelming majority of the work reviewed in Refs. 1, 2, and 15 involves bulk waves, and to a lesser extent, Rayleigh surface waves. However, over the course of the last 15 to 20 years, nonlinear ultrasonic guided waves have emerged as a powerful tool for characterization of incipient damage in structures comprised of plates, pipes/tubes, rods, and rails. The advantages of nonlinear guided waves are the union of the advantages of nonlinear ultrasonics already described (i.e., improved sensitivity and capability to detect incipient damage) and guided waves (e.g., volumetric coverage, long propagation distances, single-sided access, inspection speed, and inspection of inaccessible domains). Further advantages could be realized by implementing noncontact methods such as laser excitation and laser Doppler vibrometer measurements. However, due to the dispersive multimodal character of guided waves, they present a number of analytical challenges that bulk waves do not, and the likelihood of performing a successful inspection with nonlinear guided waves without understanding their propagation is just above nil.

In this article, theoretical modeling of nonlinear guided wave propagation is summarized first in Sec. 2. Doing so enables intelligent selection of primary wave modes that will generate strong internally resonant higher harmonics through interaction with the nonlinear elastic waveguide. Numerical simulations provide a means to test assumptions made in the model development and enable demonstration of nonlinear wave propagation features without the additional nonlinearities introduced by laboratory instrumentation. Thus, results of finite element analyses are reviewed in Sec. 3. Experiments provide the only real proof of the veracity of the theory and simulations. Thus, Sec. 4 reviews results from higher harmonic generation experiments on waveguide structures. These experimental results demonstrate...
the unique wave propagation characteristic of internally resonant higher harmonics; their cumulative nature. They also show how the higher harmonics generation changes as the material microstructure changes. The article closes with a summary and discussion of where the current state-of-knowledge could lead.

2 Theory

In Sec. 1, we provided the motivation for using nonlinear guided waves for microscale damage detection and characterization. However, the mathematical complexity associated with guided wave propagation does not easily lend itself for analysis from a theoretical standpoint. A first step in this regard was taken by Deng to analyze the second-harmonic guided wave generation from shear-horizontal (SH) and Rayleigh–Lamb (RL) modes in plates. The approach was based on the use of the partial-wave technique to expand the primary wave-field, and then to examine the conditions under which the second harmonics from partial waves generate a propagating guided wave field. De Lima and Hamilton employed a different approach to analyze second-harmonic guided wave generation in plates. In this section, we describe their approach to study second-harmonic guided wave propagation in plates. Unlike the study by De Lima and Hamilton, we adopt a displacement gradient-based formulation that enables a systematic analysis procedure. Next, we introduce some notation that is used in the rest of the article.

2.1 Notation

We used bold letters to denote vectors and tensors and denote the position of the material particle in the reference and current configurations by $\mathbf{X}$ and $\mathbf{x}$, respectively. The displacement of the material particles is denoted by $\mathbf{u}$. The deformation gradient is denoted by $\mathbf{F}$ and is given by

$$ \mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}}. \quad (1) $$

Likewise, the displacement gradient is denoted by $\mathbf{H}$ and is given by

$$ \mathbf{H} = \frac{\partial \mathbf{u}}{\partial \mathbf{X}} = \mathbf{F} - \mathbf{I}. \quad (2) $$

where $\mathbf{I}$ is the identity tensor. We use a Lagrangian measure of strain denoted by $\mathbf{E}$ and given by

$$ \mathbf{E} = \frac{1}{2} (\mathbf{F}^T \mathbf{F} - \mathbf{I}) = \frac{1}{2} (\mathbf{H} + \mathbf{H}^T + \mathbf{H}^T \mathbf{H}). \quad (3) $$

Also, the linearized strain that does not include geometric nonlinearity is denoted by $\mathbf{E}_{\text{lin}}$ and is given by

$$ \mathbf{E}_{\text{lin}} = \frac{1}{2} (\mathbf{H} + \mathbf{H}^T). \quad (4) $$

In this article, two equivalent (widely used) weakly nonlinear hyperelastic constitutive models that describe the strain energy function of the material are used and are given by

1. Landau–Lifshitz model

$$ W(\mathbf{E}) = \frac{1}{2} \lambda \text{tr}(\mathbf{E})^2 + \mu \text{tr}(\mathbf{E}^2) + \frac{1}{3} C [\text{tr}(\mathbf{E})]^3 $$

$$ + B \text{tr}(\mathbf{E}) \text{tr}(\mathbf{E}^2) + \frac{1}{3} A \text{tr}^2(\mathbf{E}). \quad (5) $$

2. Murnaghan model

$$ W(\mathbf{E}) = \frac{1}{2} \lambda \text{tr}(\mathbf{E})^2 + \mu \text{tr}(\mathbf{E}^2) + \frac{1}{3} (l + 2m) [\text{tr}(\mathbf{E})] $$

$$ + m \text{tr}(\mathbf{E}) (\text{tr}^2(\mathbf{E}^2) - \text{tr}(\mathbf{E}^2)) + n \text{det}(\mathbf{E}). \quad (6) $$

Here, $\lambda$, $\mu$ are the Lamé’s constants, $A$, $B$, $C$ are called the third order elastic constants, and $I$, $m$, $n$ are called the Murnaghan constants. The constants $(A, B, C)$ and $(I, m, n)$ are related by $l = B + C$, $m = (1/2) A + B$, and $n = A$. Next, we introduce some stress measures used in this article. First, the second Piola–Kirchhoff stress tensor $(\mathbf{T}_{\text{RR}})$ is obtained from $W(\mathbf{E})$ and is given by

$$ \mathbf{T}_{\text{RR}} = \frac{\partial W(\mathbf{E})}{\partial \mathbf{E}}. \quad (7) $$

The first Piola–Kirchhoff stress $(\mathbf{S})$ is related to $\mathbf{T}_{\text{RR}}$ by

$$ \mathbf{S} = \mathbf{F}^T \mathbf{T}_{\text{RR}}. \quad (8) $$

For the Landau–Lifshitz model, the second Piola–Kirchhoff stress tensor is written in terms of strain as

$$ \mathbf{T}_{\text{RR}}(\mathbf{E}) = \lambda \text{tr}(\mathbf{E}) \mathbf{I} + 2 \mu \mathbf{E} + C \text{tr}(\mathbf{E})^2 \mathbf{I} + B \text{tr}(\mathbf{E}^2) \mathbf{I} $$

$$ + 2 B \text{tr}(\mathbf{E}) \mathbf{E} + A \mathbf{E}^2. \quad (9) $$

Since our theoretical formulation is based on the displacement gradient, we treat first and second Piola–Kirchhoff stress tensors as explicit functions of displacement gradient $(\mathbf{H})$ and they are denoted as $(\mathbf{S}(\mathbf{H}))$ and $\mathbf{T}_{\text{RR}}(\mathbf{H})$. $\mathbf{T}_{\text{RR}}(\mathbf{H})$ can be obtained by using Eqs. (9) and (3) and is given by

$$ \mathbf{T}_{\text{RR}}(\mathbf{H}) = \frac{1}{2} \text{tr}(\mathbf{H} + \mathbf{H}^T)^2 + \mu (\mathbf{H} + \mathbf{H}^T)^2 + \frac{1}{2} \text{tr}(\mathbf{H}^T \mathbf{H}) \mathbf{I} $$

$$ + C \text{tr}(\mathbf{H})^2 \mathbf{I} + \mu \mathbf{H}^T \mathbf{H} + B \text{tr}(\mathbf{H})(\mathbf{H} + \mathbf{H}^T) $$

$$ + \frac{B}{2} \text{tr}(\mathbf{H}^2 + \mathbf{H}^T \mathbf{H}) \mathbf{I} + \frac{A}{4} (\mathbf{H}^2 + \mathbf{H}^T \mathbf{H} + \mathbf{H} \mathbf{H}^T + \mathbf{H}^T \mathbf{H}^2). \quad (10) $$

up to second order in $\mathbf{H}$. Further, we decompose $\mathbf{T}_{\text{RR}}(\mathbf{H})$ into two parts, namely $\mathbf{T}_{\text{lin}}(\mathbf{H})$ and $\mathbf{T}_{\text{nl}}(\mathbf{H})$ such that $\mathbf{T}_{\text{RR}}(\mathbf{H}) = \mathbf{T}_{\text{lin}}(\mathbf{H}) + \mathbf{T}_{\text{nl}}(\mathbf{H})$. As indicated in the notation, $\mathbf{T}_{\text{lin}}(\mathbf{H})$ is linear in $\mathbf{H}$ and $\mathbf{T}_{\text{nl}}(\mathbf{H})$ is nonlinear in $\mathbf{H}$ and is explicitly given by

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\[ T_{RR}^{L}(H) = \frac{\lambda}{2} \nabla(H + H^T) + \mu(H + H^T), \]
\[ T_{RR}^{NL}(H) = \frac{\lambda}{2} \nabla(H^T)I + C(\nabla H)^2I + \mu \nabla H^T + B(\nabla H)(H + H^T) \]
\[ \quad + \frac{B}{2} \nabla(\nabla^2 H + H^T H)I + \frac{A}{4} (H^2 + H^T H + H H^T + H^T H). \]

Likewise, using \( S = F T_{RR} \), we can write \( S(H) = S^L(H) + S^{NL}(H) \) where
\[ S^L(H) = T_{\text{RR}}^L(H), \]
and
\[ S^{NL}(H) = H T_{\text{RR}}^L(H) + T_{\text{RR}}^{NL}(H). \]

Equivalent expressions can be obtained for the Murnaghan model. However, we restrict ourselves to the Landau–Lifshitz model in this section.

\section*{2.2 Second-Harmonic Guided Waves in Plates}

Consider the schematic of the traction-free plate in the reference configuration as shown in Fig. 1. We begin with the referential form of the balance of the linear momentum given by
\[ \text{Div}[S(H)] = \rho_c \ddot{u}, \quad \text{Sn}_k = 0 \text{ on } X_2 = \pm h, \] (13)
where \( \text{Sn}_k \) denotes the unit normal to the surface of the plate in the reference configuration and \( \rho_c \) denotes the density of the material in the reference configuration.

Suppose that the displacement associated with the primary wave propagating in the plate is denoted by \( u_1(X,t) \), and that associated with the secondary wavefield is denoted by \( u_2(X,t) \), then the total displacement in the material is given by
\[ u(X,t) = u_1(X,t) + u_2(X,t) \text{ with } ||u_2|| \ll ||u_1||, \] (14)
where the perturbation assumption is indicated. Likewise for the displacement gradient, we have
\[ H = H_1 + H_2 \text{ with } ||H_2|| \ll ||H_1||, \] (15)
where \( H_1 = (\partial u_1/\partial X) \) and \( H_2 = (\partial u_2/\partial X) \) are the displacement gradients associated with primary and secondary displacements. Next, we obtain the expression for the first-Piola Kirchhoff stress that goes into Eq. (13). Using Eq. (12), we get
\[ S(H) = S^L(H) + S^{NL}(H) \Rightarrow \]
\[ S(H_1 + H_2) = S^L(H_1 + H_2) + S^{NL}(H_1 + H_2) \Rightarrow \]
\[ S(H_1 + H_2) = S^L(H_1) + S^L(H_2) + S^{NL}(H_1 + H_2), \] (16)
where the linearity of \( S^L(H) \) was used.

![Fig. 1 Cross section of the traction-free plate.](image)

As we are interested in the solution for the second harmonic, we retain only the terms of the second degree in \( H \) in the expression for \( S^{NL}(H_1 + H_2) \), and denote those terms by \( S^{NL}(H_1, H_1, 2) \) which correspond to self-interaction of the primary mode. From Eq. (16), we have
\[ S(H) = S^L(H_1) + S^L(H_2) + S^{NL}(H_1, H_1, 2). \] (17)

Substituting Eqs. (14) and (17) in Eq. (13), we obtain two separate boundary value problems for \( u_1 \) and \( u_2 \) as follows:
\[ \text{Div}[S^L(H_1)] - \rho_c \ddot{u}_1 = 0 \quad S^L(H_1) \text{ n}_k = 0, \] (18)
\[ \text{Div}[S^L(H_2)] - \rho_c \ddot{u}_2 = -\text{Div}[S^{NL}(H_1, H_1, 2)] \quad S^L(H_2) \text{ n}_k = -S^{NL}(H_1, H_1, 2) \text{ n}_k. \] (19)

Now, assume \( u_1(X,t) = \text{Re}\{u_1(X,t)e^{i(kX_1 + \omega t)}\} \), a propagating guided wave mode in the plate (can either be RL or SH mode), where \( \text{Re}\{\} \) denotes the real part of the argument, \( \omega \) denotes the angular frequency, and \( k \) denotes the wavenumber of the mode. The first problem in Eq. (18) is identically satisfied due to our assumption that \( u_1 \) is a propagating mode in the plate. On the other hand, the solution for \( u_2 \) is obtained using the normal mode expansion technique. Following De Lima and Hamilton, we seek asymptotic expansions of \( S^L(H_2) \) and \( u_2 \) as follows:
\[ S^L(H_2) = \sum_{m=1}^{m=\infty} A_m(X_1) \text{S}_m, \quad u_2 = \sum_{m=1}^{m=\infty} A_m(X_1) \text{v}_m, \] (20)
where \( \text{S}_m \) and \( \text{v}_m \) denote the stress and velocity fields corresponding to all the guided wave modes [propagating and nonpropagating (evanescent)] at \( 2\omega \).

As shown in Ref. 19, \( A_m(X_1) \) satisfies the following ordinary differential equation [Eq. (21)] for each \( n \) such that \( P_{mn} \neq 0 \)
\[ 4P_{mn} \left( \frac{\partial A_m}{\partial X_1} - ik_n X_1 \right) = (f^\text{surf} + f^\text{vol}). \] (21)

Here,
\[ P_{mn} = -\frac{1}{4} \int_{-h}^{h} \left( S_m v_n + S_n v_m \right) dX_2, \]
\[ f^\text{surf} = -\frac{1}{2} S^{NL}(H_1, H_1, 2) \text{v}_n \text{ n}_k |_{-h}^{h}, \]
\[ f^\text{vol} = \frac{1}{2} \int_{-h}^{h} \text{Div}[S^{NL}(H_1, H_1, 2)] \text{v}_n dX_2. \] (22)

For every propagating mode \( m \) used in the asymptotic expansion, there is only one propagating mode \( n = m \) such that \( P_{mn} \neq 0 \) and \( k_m = k_n \). If \( m \) corresponds to a nonpropagating mode, then \( k_m = k_n^\ast \). This ensures that the solution to Eq. (21) is well defined and is given by
\[ A_m(X_1) = -\frac{i(f^\text{surf} + f^\text{vol})}{4P_{mn}} \left( e^{ik_n X_1} - e^{ik_n X_1^\ast} \right) \text{ if } k_n^\ast \neq 2k, \]
\[ A_m(X_1) = \frac{(f^\text{surf} + f^\text{vol})}{4P_{mn}} X_1 \text{ if } k_n^\ast = 2k. \] (23)
Note that if the primary mode is a propagating mode, and if there exists another propagating mode $n = m$ such that $k_n = k_m = 2k$, then the amplitude $A_n$ increases linearly with the propagation distance and is termed as a cumulative second harmonic. While this condition is satisfied at every frequency for bulk waves, only specific primary guided wave modes generate cumulative second harmonics. The two “internal resonance” conditions that a primary mode needs to satisfy for it to generate a cumulative second harmonic are\(^{19}\)

1. Phase-matching condition: existence of a propagating guided wave mode at $(2\omega, 2k)$, where $(\omega, k)$ is the primary mode.

2. Nonzero power-flux criterion: $(f_n^{-1} + f_n^{vol}) \neq 0$ for that mode $n$ such that $k_n = k_m = 2k$.

The above analysis does not assume the nature of the primary mode and can be applied to both RL and SH modes. To identify the guided wave modes that satisfy both the conditions, one needs to analyze each of them separately as outlined below.

- Phase-matching condition\(^{19,23-26}\)
  The phase-matching condition is satisfied if and only if there exists a propagating guided wave mode in the plate at $(2\omega, 2k)$, where $(\omega, k)$ corresponds to the frequency and wavenumber of the primary mode. To proceed with the analysis, we first start with the following dispersion relations

$$\tan(qh) = \frac{4k^2 pq}{(q^2 - k^2)^2} \quad \text{(symmetric RL modes)},$$

$$\tan(qh) = \frac{4k^2 pq}{(q^2 - k^2)^2} \quad \text{(antisymmetric RL modes)},$$

$$qh = \frac{\pi n}{2} \quad \text{(shear-horizontal modes)}. \quad (24)$$

Here, $p = \sqrt{(\omega/c_l)^2 - k^2}$ and $q = \sqrt{(\omega/c_t)^2 - k^2}$, where $c_l$ and $c_t$ are the longitudinal and transverse wave speeds in the material, respectively. The phase matching condition needs to be analyzed for different combinations of primary and secondary modes. First, consider the case of a primary RL mode generating a secondary RL mode. If both the primary $(\omega, k)$ and secondary modes $(2\omega, 2k)$ are symmetric modes then we have

$$\frac{\tan(qh)}{\tan(2qh)} = \frac{\tan(2ph)}{\tan(2ph)}.$$

Likewise, we can write relations for all possible combinations of the primary and secondary RL modes as follows:

$$\frac{\tan(qh)}{\tan(ph)} = \frac{\tan(2qh)}{\tan(2ph)}.$$  
Primary symmetric (antisymmetric)

$\Rightarrow$ Secondary symmetric (antisymmetric),

$$\frac{\tan(qh)}{\tan(ph)} = \frac{\tan(2qh)}{\tan(2ph)}.$$  
Primary symmetric (antisymmetric)

$\Rightarrow$ Secondary antisymmetric (symmetric).

The first relation in Eq. (25) describes a primary mode generating a secondary mode of the same kind and the second relation describes a primary mode generating a secondary mode of the opposite kind. Similar relations can be written down for a primary SH mode generating a secondary RL mode. Care must be taken in interpreting the above relations, especially when any of the terms in the equation are $0$ or $\infty$. A detailed analysis of the phase-matching condition can be found in Refs. 23 and 24. Next, we analyze the nonzero-power-flux criterion.

- Nonzero power flux criterion\(^{16,22,25-27}\)
To analyze nonzero power flux criterion, we adopt a parity analysis in terms of the displacement gradient ($\mathbf{H}$). First, we begin by observing that the displacement field and the corresponding displacement gradient in the plate for different modes are of the following form given in Table 1. Here, S denotes a symmetric (even) function about the midplane of the plate and A denotes an antisymmetric (odd) function about the midplane of the plate.

<table>
<thead>
<tr>
<th>Primary mode</th>
<th>$u_i$ (displacement)</th>
<th>$H_i$ (displacement gradient)</th>
</tr>
</thead>
<tbody>
<tr>
<td>RL symmetric</td>
<td>$\begin{bmatrix} S \ A \ 0 \end{bmatrix}$</td>
<td>$\begin{bmatrix} S &amp; A &amp; 0 \ A &amp; S &amp; 0 \ 0 &amp; 0 &amp; 0 \end{bmatrix}$</td>
</tr>
<tr>
<td>RL antisymmetric</td>
<td>$\begin{bmatrix} A \ S \ 0 \end{bmatrix}$</td>
<td>$\begin{bmatrix} A &amp; S &amp; 0 \ S &amp; A &amp; 0 \ 0 &amp; 0 &amp; 0 \end{bmatrix}$</td>
</tr>
<tr>
<td>SH symmetric</td>
<td>$\begin{bmatrix} 0 \ 0 \ S \end{bmatrix}$</td>
<td>$\begin{bmatrix} S &amp; A &amp; 0 \ A &amp; S &amp; 0 \ 0 &amp; 0 &amp; 0 \end{bmatrix}$</td>
</tr>
<tr>
<td>SH antisymmetric</td>
<td>$\begin{bmatrix} S \ A \ 0 \end{bmatrix}$</td>
<td>$\begin{bmatrix} S &amp; A &amp; 0 \ A &amp; S &amp; 0 \ 0 &amp; 0 &amp; 0 \end{bmatrix}$</td>
</tr>
</tbody>
</table>
Correspondingly, one can show\textsuperscript{22,25} that the nonlinear terms \( S^{NL}(H_1, H_2) \) and \( \operatorname{Div}[S^{NL}(H_1, H_2)] \) are of the parity indicated in Table 2.

From the above observations, one can conclude\textsuperscript{26} the following:

1. \( f_n^{urf} = (1/2) S^{NL}(H_1, H_2) v_n n_2 \), if and only if \( v_n \) corresponds to a symmetric mode.

2. \( f_n^{vol} = (1/2) \int_0^h \operatorname{Div}[S^{NL}(H_1, H_2)] v_n dX \), if and only if \( v_n \) corresponds to a symmetric mode.

Therefore, the power-flux \( f_n^{urf} + f_n^{vol} \neq 0 \) if and only if the secondary mode is a symmetric RL mode. It should be noted that this would also be the case even if the primary mode is an SH mode.\textsuperscript{26}

From the conclusions obtained for both the phase-matching and nonzero power flux criteria, one can identify the following list (Table 3) of guided wave modes that are capable of generating cumulative second harmonics. Here, \( m, n \) denote arbitrary positive integers. In addition to the modes listed in Table 3, other modes\textsuperscript{25} like the quasi-Rayleigh modes and (high-frequency) guided wave modes near the transverse wave speeds are also capable of second-harmonic generation.

### 2.3 Mode Selection

The importance of selecting a primary mode that generates a higher harmonic with strong internal resonance was mentioned in Sec. 1, but it cannot be overemphasized. Internal resonance is the first consideration; starting with phase matching and then assessing the secondary modes that have not just nonzero power flux, but significant power fluxes.\textsuperscript{28} Other important considerations include: modal excitability given the selected transducer, proximity of nearby modes, dispersion, diffraction, and attenuation. In fact, the number of primary modes that generate internally resonant second harmonics that are measured by currently available transducers are so low that the generation of third harmonics was analyzed.\textsuperscript{29}

### 2.4 Nonlinear Guided Waves in Other Waveguides

In this section, we briefly summarize some of the earlier work concerning nonlinear guided waves in nonplate-like waveguides. Second harmonic, sum, and difference frequency generation in waveguides of arbitrary cross section was first investigated by De Lima and Hamilton.\textsuperscript{30} The conditions for internal resonance were arrived at and also second-harmonic generation in cylindrical rods and shells was numerically demonstrated. Likewise, generalized higher harmonic generation in waveguides of arbitrary cross section was investigated.\textsuperscript{31,32} Second-harmonic guided waves from axis-symmetric longitudinal modes in pipes were investigated in Ref. 33 using a large-radius asymptotic approximation for wavestructures in pipes. Limits on the thickness to diameter ratio were discussed by Chillara and Lissenden.\textsuperscript{34} It was observed that these wavestructures for pipes converge asymptotically to that of plates, hence, conclusions concerning second-harmonic generation for plates can be appropriately extended for pipes. Second-harmonic generation from axis-symmetric torsional and longitudinal modes was analyzed in Ref. 34. Recently, higher order mode interactions in pipes were studied\textsuperscript{35,36} where harmonic generation from flexural modes was analyzed as well.

### 3 Numerical Simulations

In this section, we discuss numerical simulations pertaining to nonlinear guided wave propagation in waveguides. Numerical simulations offer a convenient way to investigate the cumulative harmonic generation in waveguides and offer key insights into aspects of guided wave mode selection for efficient harmonic generation from a practical standpoint. The numerical studies enable us to alienate the nonlinear effects arising out of instrumentation and just study the effect of material nonlinearity on the wave propagation. Both semianalytical and numerical methods have successfully been employed to investigate nonlinear guided waves in waveguides.

Nucera and Lanza di Scalea\textsuperscript{39} developed a COMSOL based nonlinear semianalytical finite element (CO.NO. SAFE) to analyze synchronism conditions for mode-selection and also to determine the modal amplitude content at second harmonics in waveguides. The method was demonstrated for variety of waveguides like rail, composite laminates, reinforced concrete slab, and so on. Finite-difference-time-domain method incorporating material and geometric

<table>
<thead>
<tr>
<th>Primary mode</th>
<th>Cut-off modes</th>
<th>( a_p = c_j )</th>
<th>( a_p = \sqrt{2}c_j )</th>
<th>Mode-intersections</th>
<th>Special modes</th>
</tr>
</thead>
<tbody>
<tr>
<td>RL symmetric (( \omega ))</td>
<td>( \frac{n_0}{2} )</td>
<td>( \frac{n_0c_0}{\sqrt{c_j^2 - c_l^2}} )</td>
<td>( \frac{\sqrt{2}n_0c_0}{\sqrt{c_j^2 - c_l^2}} )</td>
<td>All</td>
<td>—</td>
</tr>
<tr>
<td>RL antisymmetric (( \omega ))</td>
<td>( \frac{(2n+1)c_0}{2} )</td>
<td>—</td>
<td>( \frac{\sqrt{2}n_0c_0}{\sqrt{c_j^2 - c_l^2}} )</td>
<td>All</td>
<td>—</td>
</tr>
<tr>
<td>SH (( \omega ))</td>
<td>( \frac{n_0}{2} )</td>
<td>( \frac{n_0c_0}{\sqrt{c_j^2 - c_l^2}} )</td>
<td>—</td>
<td>Modes that satisfy ( \frac{c_j^2 - c_l^2}{c_j^2} = \frac{\sqrt{2}}{2c_j^2} \left( \frac{c_j^2}{c_j^2} - \frac{1}{c_j^2} \right) )</td>
<td>—</td>
</tr>
</tbody>
</table>
nonlinearities was employed\textsuperscript{38} to study center-frequency dependence of cumulative harmonic generation in isotropic plates. Likewise, two local approaches, namely cellular automata finite element and local interaction simulation approach have been employed\textsuperscript{39} to study second-harmonic guided wave generation in waveguides. On the other hand, conventional finite element methods incorporating material and geometric nonlinearities were extensively used\textsuperscript{26,28,36,40–42} to study second-harmonic guided wave propagation in waveguides, especially in plates and pipes. In this section, we discuss the results from finite element simulations concerning second-harmonic guided waves in plates. First, we discuss second-harmonic guided wave generation in homogeneous, isotropic plates in Sec. 3.1, and then discuss results for second-harmonic guided waves in plates with inhomogeneous/localized nonlinearities in Sec. 3.2.

### 3.1 Second-Harmonic Guided Waves in Homogeneous Isotropic Plates

All the results presented in this section are obtained using the commercial finite element software COMSOL. Results are presented for an aluminum plate (1-mm thick) whose material properties are shown in Table 4. Figure 2 shows the schematic of the model used for simulations. The wave excitation is specified as a displacement boundary condition at \( x = 0 \) to excite the appropriate mode. Throughout this section, we denote the \( x \)-component of the displacement with “\( u \)” and the \( y \)-component of the displacement with “\( v \).” Figure 3 shows the dispersion curves for the plate along with the primary modes used for the study in red.

#### 3.1.1 Cumulative versus noncumulative second-harmonic generation

Here, we discuss and compare the second-harmonic generation from two different primary modes; \( S_0 \) mode (0.5 MHz) and the \( S_1 \) mode (3.6 MHz). For the FE discretization, triangular plane-strain elements with a maximum size of 0.1 mm are employed to discretize the domain along the wave propagation direction and a minimum of 15 elements are used along the thickness direction. A maximum time-step of 0.01 \( \mu s \) is used for the \( S_0 \) mode and 0.005 \( \mu s \) is used for the \( S_1 \) mode. Displacement amplitudes of \( 1 \times 10^{-7} \text{m} \) and \( 2 \times 10^{-8} \text{m} \) are used for the boundary conditions for the \( S_0 \) mode and the \( S_1 \) mode, respectively. This choice ensures a stress wave of a few MPa—typical of an ultrasonic wave propagating in the material. Note while the \( S_1 \) mode (3.6 MHz) satisfies the conditions of internal resonance discussed in Sec. 2.2, while the \( S_0 \) mode (0.5 MHz) does not satisfy the phase matching criterion of Sec. 2.2. The phase velocity of the primary \( S_0 \) mode (0.5 MHz) is 5.34 mm/\( \mu s \) and that of the second harmonic \( S_0 \) mode (1 MHz) is 5.27 mm/\( \mu s \). On the other hand, the phase velocity of both the primary \( S_1 \) mode (3.6 MHz) and the secondary \( S_1 \) mode (7.2 MHz) is 6.17 mm/\( \mu s \).

Figure 4 shows the amplitude of the second harmonic from the \( S_0 \) mode (0.5 MHz) and Fig. 5 shows the same for the \( S_1 \) mode (3.6 MHz) as a function of the normalized propagating distance. The normalization is carried out using the corresponding wavelength of the primary mode (\( \lambda_{S_0} = 10.68 \text{ mm} \), \( \lambda_{S_1} = 1.71 \text{ mm} \)). Clearly, the second harmonic from the \( S_0 \) mode (0.5 MHz) is not cumulative as it starts to decrease after about (\( \lambda_{S_0}/\lambda_{S_0} = 10 \)). On the other hand, the second harmonic from the \( S_1 \) mode (3.6 MHz) is cumulative and increases linearly as shown in Fig. 5. This is in agreement with the prediction from the perturbation approach presented in Sec. 2.2 that the \( S_1 \) mode (3.6 MHz) generates a cumulative second harmonic.

#### 3.1.2 Role of material and geometric nonlinearities

In this section, we compare the contribution of material and geometric nonlinearity to the second-harmonic generation. Simulations are carried out for the primary \( S_1 \) mode...
(3.6 MHz) generating a second-harmonic $S_2$ mode (7.2 MHz) for three variants of the constitutive model in Eq. (6). These are:

1. Linear elastic material (LE)—no material or geometric nonlinearities are included, i.e., $l = m = n = 0$ [Eq. (6)] and linearized strain, $E_{\text{lin}} = (1/2)(H + H^T)$ is used as a strain measure.

2. Nonlinear (NL)—both material and geometric nonlinearities are included, i.e., $l \neq 0, m \neq 0, n \neq 0$ (values from Table 1) and Lagrangian strain $(E)$ is used as a strain measure.

3. Geometrically nonlinear (NG)—only geometric nonlinearity is included, i.e., $l = m = n = 0$ and Lagrangian strain $(E)$ is used as a strain measure.

Figure 6 shows fast Fourier transforms for LE, NL, and NG cases at $x = 50$ mm from the left end of the plate. Clearly, the NL case has a much higher second harmonic for material behavior provide a very good approximation for studying nonlinear guided waves in plates.

### 3.1.3 Second-harmonic generation with group velocity mismatch

The results presented in the previous sections considered primary modes that are (almost) phase-matched to their second harmonic. To investigate the effect of group velocity mismatch on the second-harmonic generation, simulations are run for the primary $A_0$ mode (0.5 MHz). The amplitude of the displacement boundary condition is increased to $10^{-5}$ m to decipher some important aspects of second-harmonic generation as outlined later. Figure 7 shows the Hilbert transform (positive envelope) of the time-domain signals on a log-scale at $x = 40, 80, \text{ and } 120$ mm from the left end of the plate. Clearly, there are two distinct peaks corresponding to the arrival time of the pulses; the one with a larger amplitude corresponds to the primary mode and arrives later due to a smaller group velocity $(2.91 \text{ mm/μs})$, and the smaller one corresponds to the secondary mode and arrives earlier in time due to a larger group velocity $(5.12 \text{ mm/μs})$. Also, they are clearly separated with the time-difference between them increasing with increasing propagation distance. A few important observations can be made in this regard:

1. The second harmonic separates from the primary mode, the hence group velocity matching is not required for the higher harmonic generation. Note that the phase matching condition is not satisfied here. This finding, which is explained further in Ref. 40, is in direct conflict with the reasonable argument presented by Muller et al. that the primary and secondary wave packets must travel together in order for energy transfer to occur. Our explanation is that the higher harmonic is generated by the material nonlinearity with the nonlinear surface traction $f_{n}^{surf}$ and nonlinear body force $f_{n}^{vol}$ terms [Eq. (22)] acting like distributed sources in a similar way that parametric arrays use distributed nonlinearity in fluids to generate directional sound beams. Thus, we believe it is the material’s nonlinearity itself that enables the secondary wave packet to propagate and be cumulative when the internal resonance criteria are satisfied.

![Fig. 5](image1.png)

**Fig. 5** Second-harmonic amplitude ($A_2$ in m) from primary $S_1$ mode (3.6 MHz) with normalized propagation distance.

![Fig. 6](image2.png)

**Fig. 6** Primary mode: $S_1$ mode (3.6 MHz)—fast Fourier transforms (log-scale) obtained from time domain signals at $x = 50$ mm for the three cases: linear elastic material, nonlinear, and geometrically nonlinear.

![Fig. 7](image3.png)

**Fig. 7** Primary mode: $A_0$ mode (0.5 MHz)—Hilbert transform of time domain signals at $x = 40, 80, \text{ and } 120$ mm.
However, if the primary and secondary waves have different group velocities, due care must be taken in their measurement.

2. The second-harmonic mode generated is the $S_0$ mode (1 MHz) as opposed to the $A_0$ mode (1 MHz) as is evident from the through-thickness displacement profiles “v” in Fig. 8 at $x = 120$ mm during the times $t = 28$ to $35 \mu$s, which is antisymmetric about the mid-plane. This is in agreement with the predictions from the perturbation approach.

3. It can be concluded that the second harmonic is continuously generated from the primary mode and once generated, it can propagate independent of the primary mode. This can be explained with the following rationale. As observed here, the second harmonic separates from the primary mode and propagates as a distinct pulse independent of the primary mode. Now, the residual primary mode can again generate a second harmonic and this process repeats with the second-harmonic pulses being separated from the primary mode when sufficient time has elapsed—as dictated by the group velocity mismatch between the primary and the secondary modes. Also, the separated harmonic can itself generate other higher harmonics. The theory of mode interaction presented in Ref. 22 can be used to assess the nature of such a higher harmonic generation. It should be noted that these are much smaller in magnitude when compared to the primary mode and pose an enhanced difficulty in detecting them in an experiment.

3.2 Second-Harmonic Guided Waves in Plates with Inhomogeneous/Localized Nonlinearities

3.2.1 Homogeneous versus inhomogeneous nonlinearity

Here, we compare the cumulative second-harmonic generation characteristics from $S_1$ mode (3.6 MHz) for two cases, namely homogeneous and nonhomogeneous nonlinearities in the plate. For the homogeneous case, the Murnaghan constants from Table 4 were used. For the nonhomogeneous case, the parameters $\lambda$ and $\mu$ in Table 4 were used and the Murnaghan constants were varied along the wave propagation direction ($x$). The variation is assumed to be linear, such as for a functionally graded material i.e., $l(x) = -250(1 + x/25)$ GPa, $m(x) = -333(1 + x/25)$ GPa, and $n(x) = -350(1 + x/25)$ GPa, where “$x$” is in “mm” so that the Murnaghan constants at $x = 50$ mm are three times those at $x = 0$ mm. Figure 9 shows the amplitude of the second harmonic with normalized propagation distance. Clearly, the amplitude of the second harmonic for the inhomogeneous case is much higher due to the higher nonlinearity. Also, it should be noted that the cumulative second-harmonic generation is not linear (but super-linear) as for the homogeneous case.

3.2.2 Effect of localized through-thickness nonlinearity on cumulative second-harmonic generation

In Sec. 3.2.1, we investigated the effect of inhomogeneous nonlinearity along the wave propagation direction. Now, we investigate the effect of localized through-thickness nonlinearity on the second-harmonic generation of guided waves, such as may be the case in a one-sided degradation process. Simulations are run for two primary modes, namely, the $S_0$ mode (0.5 MHz) and the $S_1$ mode (3.6 MHz). Localized nonlinearity in the model is obtained by varying the percentage through-thickness nonlinearity as indicated in the Fig. 10, where “LE” denotes LE and “NL” denotes nonlinear elastic material. The results presented in this section are from Ref. 41.

$S_0$ mode (0.5 MHz). We first present the results obtained for second-harmonic generation from the $S_0$ mode at 0.5 MHz. Figure 11 shows the relative nonlinearity parameter ($A_2/A_1^2$) at $x = 100$ mm versus the percentage through-thickness of nonlinearity. Clearly, it increases linearly with the amount of through-thickness nonlinearity. Also, Fig. 12 shows the relative nonlinearity parameter as a function of the propagating distance for varying levels of through-thickness nonlinearity. As can be seen, the nonlinearity parameter increases with the propagation distance for each of the cases. Moreover, the rate of increase of the nonlinearity parameter increases with increasing through-thickness nonlinearity.
Also, it should be noted that the 20%–20% case which corresponds to 20% nonlinearity on the top and 20% nonlinearity on the bottom of the plate almost coincides with the case with 40% nonlinearity on the top. Hence, it appears that the second-harmonic generation from the $S_0$ mode (0.5 MHz) is independent of the through-thickness damage location, but only depends on the volume-fraction of the nonlinear material. This is clearly evident from the plots of the normalized relative nonlinearity parameter shown in Fig. 13 where each curve is normalized with its value at $x = 20$ mm and all of them except one (20%) coincide. This is because, for the 20% case, the energy from the primary mode is transferred to the antisymmetric mode at the second harmonic in addition to the symmetric mode. This occurs due to the asymmetry of the material parameters in the top and bottom surfaces of the plate in Fig. 10.

It should be noted that the second-harmonic generation from the $S_0$ mode (0.5 MHz) is independent of the location of the damage due to its uniform wavestructure through the thickness as indicated in Fig. 10.

Next, we present the results obtained for second-harmonic generation from the $S_1$ mode at 3.6 MHz.

$S_1$ mode (3.6 MHz). Simulations similar to the one for the $S_0$ mode (0.5 MHz) are run for the $S_1$ mode (3.6 MHz) by varying the through-thickness nonlinearity in the plate. Simulations were run for different cases of through-thickness nonlinearity, namely, 20%, 40%, 60%, 80%, 90%, 100%, and 20%–20%, which again corresponds to 20% through-thickness damage on the top and 20% on the bottom. Unlike the $S_0$ mode (0.5 MHz), the wavestructure for the $S_1$ mode is not uniform through the thickness as indicated in the Fig. 15, which depicts the wavestructures of both the $S_1$ mode (3.6 MHz) and the $S_2$ mode (7.2 MHz). Hence, we expect the results to be different from those obtained for the $S_0$ mode (0.5 MHz).

Figure 16 shows the relative nonlinearity parameter as a function of the propagation distance. Several observations are made in this regard.

1. Relative nonlinearity parameter is much higher when compared to that from the $S_0$ mode (0.5 MHz) due to the higher frequency and cumulative nature of the $S_1$ mode (3.6 MHz).

2. Relative nonlinearity parameter is not monotonic with the increasing volume-fraction of the through-thickness damage. Hence, it can be concluded that the second-harmonic generation from the $S_1$ mode (3.6 MHz)
is not exclusively dependent on the volume fraction of through-thickness nonlinearity.

3. The case of 20%–20% coincides with that for 100%, hence it can be concluded that the second-harmonic generation is mainly due to the contribution from the material near the surface rather than that from the central portion (bulk) of the plate. In fact, it appears that the bulk contribution reduces the second-harmonic generation a little as is evident from Fig. 16 where the 20%–20% case surpasses the 100% for $x > 30$ mm.

From the above study, it appears that the second-harmonic generation from the $S_1 - S_2$ mode pair at the longitudinal wave speed is more sensitive to the surface damage and can be used to efficiently detect and characterize it.

### 4 Experiments

Naturally, experiments are a vital part of the development of nonlinear ultrasonic guided wave-based techniques for characterization of material microstructure evolution. Even more so than for linear ultrasonic guided waves, the probability of successful experiments is low unless the nonlinear guided wave propagation characteristics are understood and used to select modes, frequencies, and transducers that activate primary waves that, in turn, generate strong cumulative higher harmonics. This section starts by describing general considerations for nonlinear ultrasonic guided wave experiments intended to measure the generation of higher harmonics. It then reviews experimental results that have been reported in the literature.

#### 4.1 Measurement Considerations

The first and foremost experimental consideration is that a finite amplitude near-monochromatic waveform having excellent clarity is actuated. Three issues are embedded in this consideration: (1) finite amplitude is desirable in order that the generated higher harmonics, which have far less energy than the primary wave, are measurable; (2) the tail of the frequency distribution can overwhelm the higher harmonics unless a narrow bandwidth excitation is obtained, thus a toneburst excitation having a large number of cycles is typical; and (3) high-signal clarity, or lack of distortion, reduces the noise in the frequency spectrum making the very low amplitude higher harmonics generated by the material more evident. These issues apply to bulk waves and guided waves, but because guided waves are multimodal, it is even more important to get as much energy as possible into the selected primary wave mode at the frequency that will generate the higher harmonic of interest. The second consideration, which is linked to the first, is the intrinsic nonlinearity of the measurement system. A typical measurement system comprises: synthesizer, amplifier, cables, transmit transducer, coupling media, test material, more coupling media, receive transducer, cabling, preamplifier, and oscilloscope. Matching networks and filters are also often used to improve system performance. It is important that the signal distortion due to the material nonlinearity dominates the distortion associated with other elements in the measurement system. The considerations described above are always a concern, but specific experimental setups will have additional considerations. For example, the ability to separate the transmitter and receiver by different distances enables the cumulative nature of higher harmonic waves to be assessed. Hence, it provides confirmation that the distortion causing higher harmonic generation is associated with the material.

#### 4.2 Transducers

Once a primary mode and the higher harmonic that it generates have been selected, transducers can be chosen to...
transmit and receive based on mode excitability. The wave-
structure (i.e., transverse resonance pattern) for the selected
primary mode and frequency dictates the effectiveness of a
transducer to actuate that mode. The proximity of other
modes to the frequency/wavenumber of the selected mode
and their excitability dictates how preferentially the selected
primary mode is actuated with respect to the other modes.
Similar considerations apply to receiving the higher har-
monic mode. Waves actuated from finite-size transmitters
will diffract, which was not modeled in Sec. 2. Material
attenuation was not modeled either, thus the linear cumula-
tive effect of higher harmonics given by Eq. (22) for inter-
nally resonant mode pairs is not attained due to diffraction
and attenuation. Note that internal resonance is not required
for higher harmonic generation, but it is required for the
higher harmonic to be cumulative. Preferred transmitters
have a large footprint to minimize diffraction, strong cou-
pling between the electrical signal and resulting mechanical
disturbance, and minimal distortion of the waveform. Many
researchers choose to minimize distortion at the expense
of strong coupling by choosing single crystal lithium niobate
instead of polycrystalline lead zirconate titanate (PZT) for
piezoelectric transducers. Preferential excitation of guided
wave modes can be achieved with angle beam transducers
and comb (or interdigital) transducers regardless of the type
of transduction. The means of coupling the transmitter to the
material is important because conventional gel couplant
attenuation was not modeled either, thus the linear cumula-
tion on which they superimposed the group velocity
dispersion curves as shown in Fig. 18. In this case, the
group velocities of the $S_1$ and $S_2$ modes are well matched
(4.3 mm/µs). Bermes et al.\textsuperscript{47} then expand their analysis to
include the primary $S_2$ mode, also at $c_p = c_l$, and the $S_4$
secondary mode. The use of a laser interferometer to receive the
wave signals has several advantages that include: flat fre-
cquency response, no averaging affects from a finite size
receiver, and because it is a noncontact measurement, it is
easy to change the propagation distance.\textsuperscript{46,47}

Matlack et al.\textsuperscript{48} performed a comparative study of three
internally resonant mode pairs ($S_1 - S_2$, $S_2 - S_4$, and
$A_2/S_2 - S_4$) with the result that the $S_1 - S_2$ mode pair is
preferred for practical reasons, but since the $S_2 - S_4$ mode pair
has a higher $\beta'$, it would be preferred given more effective
experimental procedures (i.e., it is difficult to preferentially
activate the $S_2$ mode at $c_p = c_l$). Pruell et al.\textsuperscript{49,50} com-
pared the use of an angle beam receiver with laser interferometer
reception for an aluminum plate that was plastically
deformed. They found that $\beta'$ increased initially due to plas-
tic deformation and then remained relatively constant. The $\beta''$
values obtained from the laser interferometer were lower
than those from the angle beam receiver because the piezo-
electric transducer used for the angle beam was selected to
preferentially receive the second-harmonic frequency, and
therefore, partially filtered the primary wave. Pruell et al.\textsuperscript{31}
showed that $\beta''$ increases with low-cycle fatigue for the $S_1 - S_2$
mode pair. Cycling was performed in load control and the maximum plastic strain was less than
0.02 m/m after 50 cycles, which gave an increase of 17%
in $\beta$. From a theoretical perspective, it is surprising that Lee et al.\textsuperscript{52} found the $A_1 - A_2$ mode pair to give a second harmonic that increased with the propagation length. Liu et al.\textsuperscript{53} compared second-harmonic measurements of antisymmetric modes with symmetric modes and found them to be significantly smaller, but not zero.

### 4.4.2 Magnetostrictive transducers

A magnetostrictive transducer (MST) consisting of a magnetostrictive (e.g., iron-cobalt) foil, a meandering electric coil, and a permanent magnet functions similar to a comb transducer, in that the coil spacing dictates the preferred wavelength. The foil is typically coupled to the plate by adhesive bonding. By orienting the permanent magnetic field bias collinear with the electric current in the coil, SH wave modes are activated/received, while orienting it perpendicular results in RL wave modes. Liu et al.\textsuperscript{26} showed that the internally resonant $SH_3 - S_4$ mode pair is cumulative and detectable with MSTs. The MST transmitter was configured to send the $SH_3$ mode at frequency $f_0 = 2.63$ MHz, while the MST receiver was configured to receive the $S_4$ RL mode at $2f_0$. Due to the finite size of the MSTs, energy was received at both the primary and second-harmonic frequencies. Energy was received at the primary frequency because the wavefront was curved, thus creating a detectable RL component from the primary SH wave. Finite element simulations were conducted to demonstrate this by investigating 20 and 100 mm wide MSTs. Lissenden et al.\textsuperscript{54} showed that the third harmonic of the fundamental $SH_0$ mode is quite sensitive to plastic deformation. In this investigation, 2024-T3 aluminum plates were plastically deformed within a reduced width region having lengths of $L = 51$, 102, 229, and 457 mm. The wave propagation distance was 430 mm, thus the plastic strain localization increased as $L$ decreased, even though it was reasonably uniform (i.e., 5\% to 8\%) over the distance $L$. The modal amplitude ratio, $A_3/A_1$, was 4.8 times larger for a uniformly deformed plate than it was for an undeformed plate. As the localization increased, the $A_3/A_1$ decreased linearly until it was indistinguishable from the undeformed plate for a localization-to-propagation distance ratio of 0.12. Furthermore, the plastic strain level was shown to have a significant effect on the modal amplitude ratio, $A_3/A_1$. In the related experiments presented by Lissenden et al.\textsuperscript{55} using load-controlled cycling to fatigue smooth-sided plate samples, the modal amplitude ratio increased by a factor of 3.6 at 80\% of the fatigue life relative to the pristine material.

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Fig. 17 (a) Primary and second harmonic amplitudes and (b) relative nonlinearity parameter with the propagation distance. (Reprinted from Ref. 44 with the permission of authors and AIP Publishing.)

Fig. 18 Spectrogram showing the amplitudes and time of arrival of the primary and secondary modes. (Reprinted from Ref. 46 with permissions from authors and AIP Publishing.)
No fatigue cracks were visually evident. Thus, the large change in the modal amplitude ratio has a strong potential to represent material degradation prior to initiation of a macroscale crack.

4.4.3 Disc transducers
PZT disc transducers are inexpensive and easily surface-bonded to take advantage of the shear stress activated in the adhesive associated with radial resonance of the disc. However, mode control capabilities are very limited. Hong et al.\textsuperscript{56} reported $\beta^\prime$ for a pristine aluminum plate that appears to increase linearly with propagation distance. However, the PZT disc actuator actuates a circular crested wave whose primary amplitude decreases as $1/\sqrt{r}$ with propagation distance, so it is likely that the results are significantly affected by the primary wavefront spreading. Hong et al.\textsuperscript{56} also investigated the effect of a small fatigue crack on $\beta^\prime$ with PZT discs and finite element modeling that includes material nonlinearity as well as contact acoustic nonlinearity (CAN) from opening and closing of the crack. The authors plotted $\beta^\prime$ as a function of distance from the crack as shown in Fig. 10 of Hong et al.\textsuperscript{56} In the experiment, a 4-mm long high-cycle fatigue crack half way through the thickness of the plate was initiated in a single edge notch sample. Material plasticity associated with dislocation dipoles was included in the model, but since the authors do not discuss the plastic zone size, it is implied that the material is modeled as being homogeneous. If this is, indeed, the case, then the results indicate that the CAN dominates the material nonlinearity, otherwise $\beta^\prime$ would not have decreased for wave paths located further from the crack. Hong et al.\textsuperscript{57} use second harmonics for imaging fatigue damage at a rivet hole by using an array of disc transducers.

We note that CAN associated with breathing cracks has been studied by numerous researchers using sub- and super-harmonic generation methods.\textsuperscript{58-61}

4.5 Other Waveguides (Composite Plate, Pipes, Rods, and Rail)
While the majority of the nonlinear guided wave experiments were conducted on metal plates, other nondestructive evaluation applications of note are briefly mentioned. Second-harmonic generation in unidirectional composite plates subjected to thermal and impact damage was studied in Refs. 62 and 63, respectively. Li and Cho\textsuperscript{64} also measured second-harmonic generation in a pipe. Choi et al.\textsuperscript{65} used the axisymmetric $T(0,1)$ mode in an Alloy 617 pipe to generate third harmonics that are sensitive to the fatigue-creep damage that was present. Nucera and Lanza di Scalea\textsuperscript{66} investigated nonlinear guided waves in solids subjected to constrained thermal expansion with a view of being able to characterize residual stresses due to the thermal expansion of rails.

5 Conclusions
Material and geometric nonlinearities distort passing guided waves, which cause self-interactions to generate higher harmonics at integer multiples of the excitation frequency and mutual interactions to generate combinational harmonics. Because propagating guided waves are confined to the dispersion curves, the selection of primary modes that generates internally resonant higher harmonics is a critical first step that has been enabled by theoretical modeling. Internally resonant mode pairs are phase matched and have nonzero power flux, and unfortunately, are quite limited in number. Numerical simulations enable virtual experiments to be conducted without instrument nonlinearities and collection of data that is difficult to acquire from physical experiments. Simulations have shown that secondary modes once generated, propagate independent of the primary mode without the need for group velocity matching. Also, it was found that the interplay between the wavestructure of the primary mode and localized material degradation significantly affects the harmonic generation. Experiments have been conducted with a variety of transmitters and receivers that demonstrate the relevant features of higher harmonic guided waves: e.g., antisymmetric second-harmonic RL modes are not cumulative while symmetric second-harmonic RL modes are, and they are sensitive to various types of microstructural evolution. Thus, nonlinear guided waves have a strong potential for characterization of incipient damage. In order to achieve the potential of nonlinear guided waves, it seems expedient to correlate the higher harmonic generation with actual features of the material microstructure. Investigations to relate ultrasonic nonlinearity for bulk waves with material microstructure have been reported by numerous researchers.\textsuperscript{12,14,43,67,68} However, these 1-D analysis efforts may not be applicable for guided waves due to their three-dimensional nature. Recent investigations by the authors define an asymmetry parameter for mesoscale analysis that can be homogenized up to the continuum level.\textsuperscript{59,60} More research along these lines should enable a correlation between the higher harmonic generation and the evolution of the microstructure, which is incipient damage. This, in turn, will enable remaining life prediction at an early point in the service life of structural systems.

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Chilhara and Lissenden: Review of nonlinear ultrasonic guided wave nondestructive evaluation...


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